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OPERATING RECOMMENDATIONS

OIL TYPE

Hydraulic oils with anti-wear, anti-foam and demulsifiers are recommended for systems incorporating Impro Fluidtek motors. Straight oils can be used but may require VI (viscosity index) improvers depending on the operating temperature range of the system. Other water based and environmentally friendly oils may be used, but service life of the motor and other components in the system may be significantly shortened. Before using any type of fluid, consult the fluid requirements for all components in the system for compatibility. Testing under actual operating conditions is the only way to determine if acceptable service life will be achieved.

FLUID VISCOSITY & FILTRATION

Fluids with a viscosity between 20 - 43 cSt [100 - 200 S.U.S.] at operating temperature is recommended. Fluid temperature should also be maintained below 85°C [180° F]. It is also suggested that the type of pump and its operating specifications be taken into account when choosing a fluid for the system. Fluids with high viscosity can cause cavitation at the inlet side of the pump. Systems that operate over a wide range of temperatures may require viscosity improvers to provide acceptable fluid performance.

Impro Fluidtek recommends maintaining an oil cleanliness level of ISO 17-14 or better.

INSTALLATION & START-UP

When installing an Impro Fluidtek motor it is important that the mounting flange of the motor makes full contact with the mounting surface of the application. Mounting hardware of the appropriate grade and size must be used. Hubs, pulleys, sprockets and couplings must be properly aligned to avoid inducing excessive thrust or radial loads. Although the output device must fit the shaft snug, a hammer should never be used to install any type of output device onto the shaft. The port plugs should only be removed from the motor when the system connections are ready to be made. To avoid contamination, remove all matter from around the ports of the motor and the threads of the fittings. Once all system connections are made, it is recommended that the motor be run-in for 15-30 minutes at no load and half speed to remove air from the hydraulic system.

MOTOR PROTECTION

Over-pressurization of a motor is one of the primary causes of motor failure. To prevent these situations, it is necessary to provide adequate relief protection for a motor based on the pressure ratings for that particular model. For systems that may experience overrunning conditions, special precautions must be taken. In an overrunning condition, the motor functions as a pump and attempts to convert kinetic energy into hydraulic energy. Unless the system is properly

configured for this condition, damage to the motor or system can occur. To protect against this condition a counterbalance valve or relief cartridge must be incorporated into the circuit to reduce the risk of over-pressurization. If a relief cartridge is used, it must be installed upline of the motor, if not in the motor, to relieve the pressure created by the over-running motor. To provide proper motor protection for an over-running load application, the pressure setting of the pressure relief valve must not exceed the intermittent rating of the motor.

HYDRAULIC MOTOR SAFETY PRECAUTION

A hydraulic motor must not be used to hold a suspended load. Due to the necessary internal tolerances, all hydraulic motors will experience some degree of creep when a load induced torque is applied to a motor at rest. All applications that require a load to be held must use some form of mechanical brake designed for that purpose.

MOTOR/BRAKE PRECAUTION

Caution! - Impro Fluidtek motor/brakes are intended to operate as static or parking brakes. System circuitry must be designed to bring the load to a stop before applying the brake.

Caution! - Because it is possible for some large displacement motors to overpower the brake, it is critical that the maximum system pressure be limited for these applications. Failure to do so could cause serious injury or death. When choosing a motor/brake for an application, consult the performance chart for the series and displacement chosen for the application to verify that the maximum operating pressure of the system will not allow the motor to produce more torque than the maximum rating of the brake. Also, it is vital that the system relief be set low enough to insure that the motor is not able to overpower the brake.

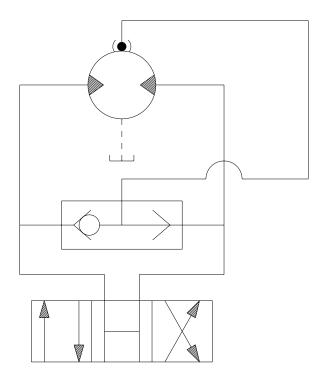
To ensure proper operation of the brake, a separate case drain back to tank must be used. Use of the internal drain option is not recommended due to the possibility of return line pressure spikes. A simple schematic of a system utilizing a motor/brake is shown on page 5. Although maximum brake release pressure may be used for an application, a 34 bar [500 psi] pressure reducing valve is recommended to promote maximum life for the brake release piston seals. However, if a pressure reducing valve is used in a system which has case drain back pressure, the pressure reducing valve should be set to 34 bar [500 psi] over the expected case pressure to ensure full brake release. To achieve proper brake release operation, it is necessary to bleed out any trapped air and fill brake release cavity and hoses before all connections are tightened. To facilitate this operation, all motor/brakes feature two release ports. One or both of these ports may be used to release the brake in the



OPERATING RECOMMENDATIONS & MOTOR CONNECTIONS

MOTOR/BRAKE PRECAUTION

unit. Motor/brakes should be configured so that the release ports are near the top of the unit in the installed position.



Once all system connections are made, one release port must be opened to atmosphere and the brake release line carefully charged with fluid until all air is removed from the line and motor/brake release cavity. When this has been accomplished the port plug or secondary release line must be reinstalled. In the event of a pump or battery failure, an external pressure source may be connected to the brake release port to release the brake, allowing the machine to be moved.

▶ NOTE: It is vital that all operating recommendations be followed. Failure to do so could result in injury or death.

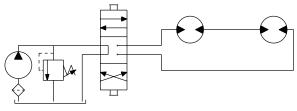
MOTOR CIRCUITS

There are two common types of circuits used for connecting multiple numbers of motors – series connection and parallel connection.

SERIES CONNECTION

When motors are connected in series, the outlet of one motor is connected to the inlet of the next motor. This allows the full pump flow to go through each motor and provide maximum speed. Pressure and torque are distributed between the motors based on the load each motor is

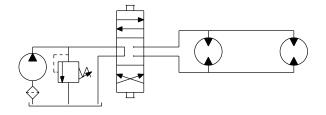
to. The maximum system pressure must be no greater than the maximum inlet pressure of the first motor. The allowable back pressure rating for a motor must also be considered. In some series circuits the motors must have an external case drain connected. A series connection is desirable when it is important for all the motors to run the same speed such as on a long line conveyor.



SERIES CIRCUIT

PARALLEL CONNECTION

In a parallel connection all of the motor inlets are connected. This makes the maximum system pressure available to each motor allowing each motor to produce full torque at that pressure. The pump flow is split between the individual motors according to their loads and displacements. If one motor has no load, the oil will take the path of least resistance and all the flow will go to that one motor. The others will not turn. If this condition can occur, a flow divider is recommended to distribute the oil and act as a differential.



PARALLEL CIRCUIT

▶ NOTE: The motor circuits shown above are for illustration purposes only. Components and circuitry for actual applications may vary greatly and should be chosen based on the application.



PRODUCT TESTING

Performance testing is the critical measure of a motor's ability to convert flow and pressure into speed and torque. All product testing is conducted using an Impro Fluidtek state of the art test facility. This facility utilizes fully automated test equipment and custom designed software to provide accurate, reliable test data. Test routines are standardized, including test stand calibration and stabilization of fluid temperature and viscosity, to provide consistent data. The example below provides an explanation of the values pertaining to each heading on the performance chart.

			Pressure - ba	rs [psi]					Max. Cont.	Max. Inter.			
	080		17 [250]	35 [500]	69 [1000]	104 [150	38 [2000]	173 [2500]	207 [3000]	242 [3500]			
	cc [4.6 in ³ /r	ev.]	rque - Nm [lb-in], Speed	rpm				Intermitter	nt Ratings - 10	0% of O	peration	
Flow - lpm [gpm]	2 [0.5]	(14 [127] 25	30 [262] 24	61 [543] 21	91 [806] 18	120 [1062] 17	145 [1285] 11	169 [1496] 11	191 [1693] 9		26	Theo
md ₁ -	4 [1]		16 [140] 50	32 [286] 50	63 [559] 43	95 [839] 43	124 [1099] 34	151 [1340] 32	178 [1579] 32	31		51	Theoretical rpm
Flow .	8 [2]		16 [139] 100	32 [280] 100	64 [563] 99	97 [857] 92	129 [1139] 87	157 [1390] 79	187 [1652] 78	211 [1865] 77	L	101	rpm
	15 [4]		14 [127] 200	31 [275] 200	65 [572] 199	99 [872] 191	131 [1155] 181	160 [1420] 174	186 [1643] 160	216 [1911] 154		201	
	23 [6]		13 [113] 301	30 [262] 300	63 [557] 297	96 [853] 295	130 [1149] 284	160 [1420] 271	186 [164 253	3 18 [1930] 245		302	
	1		10 [91] 401	27 [243] 400	61 [536] 398	93 [826] 390	127 [1125] 384	159 [1409] 372	187 [1654] 346	220 [1945] 339		4	
	38 [10]			24 [212] 502	58 [511] 500	89 [790] 499	123 [1087] 498	156 [1379] 485	185 [1638] 443	213 [1883] 433		503	
	45 [12]			20 [177] 602	54 [482] 601	87 [767] 600	120 [1060] 597	164 [1451] 540	193 [1711] 526	228 [2021] 510		603	
Max. Cont.	53 [14]			14 [127] 690	50 [445] 689	84 [741]	124 [1098] 658	155 [1369] 644	185 [1640] 631	217 [1918] 613		704	
	61 [16]											804	
Max. Inter.	64 [17]											904	
Overall Efficiency - 70 - 100% 40 - 69% 0 - 39%													
			Theoretical To	orque - Nm [lb	-in]								
			21 [183]	41 [366]	83 [732]	124 [109	66 [1465]	207 [1831]	248 [2197]	290 [2564]			
	Displacement tested at 54°C [129°F] with an oil viscosity of 46cSt [213 SUS]												

- 1. Flow represents the amount of fluid passing through the motor during each minute of the test.
- Pressure refers to the measured pressure differential between the inlet and return ports of the motor during the test.
- 3. The maximum continuous pressure rating and maximum intermittent pressure rating of the motor are separated by the dark lines on the chart.
- Theoretical RPM represents the RPM that the motor would produce if it were 100% volumetrically efficient. Measured RPM divided by the theoretical RPM give the actual volumetric efficiency of the motor.
- 5. The maximum continuous flow rating and maximum intermittent flow rating of the motor are separated by the dark line on the chart.

- Performance numbers represent the actual torque and speed generated by the motor based on the corresponding input pressure and flow. The numbers on the top row indicate torque as measured in Nm [lb-in], while the bottom number represents the speed of the output shaft.
- 7. Areas within the white shading represent maximum motor efficiencies.
- Theoretical Torque represents the torque that the motor would produce if it were 100% mechanically efficient. Actual torque divided by the theoretical torque gives the actual mechanical efficiency of the motor.



ALLOWABLE BEARING & SHAFT LOADING

This catalog provides curves showing allowable radial loads at points along the longitudinal axis of the motor. They are dimensioned from the mounting flange. Two capacity curves for the shaft and bearings are shown. A vertical line through the centerline of the load drawn to intersect the x-axis intersects the curves at the load capacity of the shaft and of the bearing.

In the example below the maximum radial load bearing rating is between the internal roller bearings illustrated with a solid line. The allowable shaft rating is shown with a dotted line.

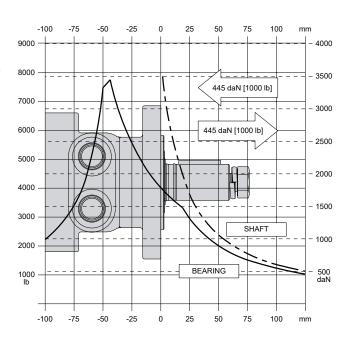
The bearing curves for each model are based on laboratory analysis and testing results constructed at Impro Fluidtek. The shaft loading is based on a 3:1 safety factor and 330 Kpsi tensile strength. The allowable load is the lower of the curves at a given point. For instance, one inch in front of the mounting flange the bearing capacity is lower than the shaft capacity. In this case, the bearing is the limiting load. The motor user needs to determine which series of motor to use based on their application knowledge.

ISO 281 RATINGS VS. MANUFACTURERS RATINGS

Published bearing curves can come from more than one type of analysis. The ISO 281 bearing rating is an international standard for the dynamic load rating of roller bearings. The rating is for a set load at a speed of 33 1/3 RPM for 500 hours (1 million revolutions). The standard was established to allow consistent comparisons of similar bearings between manufacturers. The ISO 281 bearing ratings are based solely on the physical characteristics of the bearings, removing any manufacturers specific safety factors or empirical data that influences the ratings.

Manufacturers' ratings are adjusted by diverse and systematic laboratory investigations, checked constantly with feedback from practical experience. Factors taken into account that affect bearing life are material, lubrication, cleanliness of the lubrication, speed, temperature, magnitude of the load and the bearing type.

The operating life of a bearing is the actual life achieved by the bearing and can be significantly different from the calculated life. Comparison with similar applications is the most accurate method for bearing life estimations.



EXAMPLE LOAD RATING FOR MECHANICALLY RETAINED NEEDLE ROLLER BEARINGS

Bearing Life L ₁₀ =	(C/P) ^p [10 ⁶ revolutions]
--------------------------------	--

L₁₀ = nominal rating life
C = dynamic load rating
P = equivalent dynamic load

Life Exponent p = 10/3 for needle bearings

BEARING LOAD MULTIPLICATION FACTOR TABLE				
RPM	FACTOR	RPM	FACTOR	
50	1.23	500	0.62	
100	1.00	600	0.58	
200	0.81	700	0.56	
300	0.72	800	0.50	
400	0.66			

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VEHICLE DRIVE CALCULATIONS

When selecting a wheel drive motor for a mobile vehicle, a number of factors concerning the vehicle must be taken into consideration to determine the required maximum motor RPM, the maximum torque required and the maximum load each motor must support. The following sections contain the necessary equations to determine this criteria. An example is provided to illustrate the process.

Sample application (vehicle design criteria)

vehicle description	4 wheel vehicle
vehicle drive	2 wheel drive
GVW	1,500 lbs.
weight over each drive wheel	425 lbs.
rolling radius of tires	16 in.
desired acceleration	
top speed	5 mph
gradability	20%
worst working surface	

To determine maximum motor speed

	2.65 x KPH x G	RPM =	168 x MPH x G
RPM =	rm	RPIVI -	ri

Where:

MPH = max. vehicle speed (miles/hr)
KPH = max. vehicle speed (kilometers/hr)
ri = rolling radius of tire (inches)
G = gear reduction ratio (if none, G = 1)

rm = rolling radius of tire (meters)

Example RPM =
$$\frac{168 \times 5 \times 1}{16}$$
 = 52.5

To determine maximum torque requirement of motor

To choose a motor(s) capable of producing enough torque to propel the vehicle, it is necessary to determine the Total Tractive Effort (TE) requirement for the vehicle. To determine the total tractive effort, the following equation must be used:

Where:

TE = Total tractive effort

RR = Force necessary to overcome rolling resistance

GR = Force required to climb a grade FA = Force required to accelerate

DP = Drawbar pull required

The components for this equation may be determined using the following steps:

Step One: Determine Rolling Resistance

Rolling Resistance (RR) is the force necessary to propel a vehicle over a particular surface. It is recommended that the worst possible surface type to be encountered by the vehicle be factored into the equation.

$$RR = \frac{GVW}{1000} \times R \text{ (lb or N)}$$

Where:

GVW = gross (loaded) vehicle weight (lb or kg)
R = surface friction (value from Table1)

Example RR =
$$\frac{1500}{1000}$$
 x 22 lbs = 33 lbs

Table 1

Rolling Resistance
Concrete (excellent)10
Concrete (good)15
Concrete (poor)20
Asphalt (good)12
Asphalt (fair)17
Asphalt (poor)22
Macadam (good)15
Macadam (fair)22
Macadam (poor)37
Cobbles (ordinary)55
Cobbles (poor)37
Snow (2 inch)25
Snow (4 inch)37
Dirt (smooth)25
Dirt (sandy)37
Mud37 to 150
Sand (soft)60 to 150
Sand (dune)160 to 300

Step Two: Determine Grade Resistance

Grade Resistance (GR) is the amount of force necessary to move a vehicle up a hill or "grade." This calculation must be made using the maximum grade the vehicle will be expected to climb in normal operation.

To convert incline degrees to % Grade:
% Grade = [tan of angle (degrees)] x 100

$$GR = \frac{\% \text{ Grade}}{100} \times GVW \text{ (lb or N)}$$

Example GR =
$$\frac{20}{100}$$
 x 1500 lbs = 300 lbs



VEHICLE DRIVE CALCULATIONS

Step Three: Determine Acceleration Force

Acceleration Force (FA) is the force necessary to accelerate from a stop to maximum speed in a desired time.

$$FA = \frac{MPH \times GVW \text{ (lb)}}{22 \times t} \qquad FA = \frac{KPH \times GVW \text{ (N)}}{35.32 \times t}$$

Where:

t = time to maximum speed (seconds)

Example FA =
$$\frac{5 \times 1500 \text{ lbs}}{22 \times 10}$$
 = 34 lbs

Step Four: Determine Drawbar Pull

Drawbar Pull (DP) is the additional force, if any, the vehicle will be required to generate if it is to be used to tow other equipment. If additional towing capacity is required for the equipment, repeat steps one through three for the towable equipment and sum the totals to determine DP.

Step Five: Determine Total Tractive Effort

The Tractive Effort (TE) is the sum of the forces calculated in steps one through three above. On low speed vehicles, wind resistance can typically be neglected. However, friction in drive components may warrant the addition of 10% to the total tractive effort to insure acceptable vehicle performance.

$$TE = RR + GR + FA + DP (lb or N)$$

Example TE =
$$33 + 300 + 34 + 0$$
 (lbs) = 367 lbs

Step Six: Determine Motor Torque

The Motor Torque (T) required per motor is the Total Tractive Effort divided by the number of motors used on the machine. Gear reduction is also factored into account in this equation.

$$T = \frac{TE \ xri}{M \ x \ G} \ \text{lb-in per motor} \ T = \frac{TE \ x \ rm}{M \ x \ G} \ \text{Nm per motor}$$

Where:

M = number of driving motors

Example
$$T = \frac{367 \times 16}{2 \times 1}$$
 lb-in/motor = 2936 lb-in

Step Seven: Determine Wheel Slip

To verify that the vehicle will perform as designed in regards to tractive effort and acceleration, it is necessary to calculate wheel slip (TS) for the vehicle. In special cases, wheel slip may actually be desirable to prevent hydraulic system overheating and component breakage should the vehicle become stalled.

$$TS = \frac{W \times f \times ri}{G} \qquad TS = \frac{W \times f \times rm}{G}$$
(Ib-in per motor) (N-m per motor)

Where:

f = coefficient of friction (see table 2)

W = loaded vehicle weight over driven wheel (lb or N)

Example TS =
$$\frac{425 \times .06 \times 16}{1}$$
 lb-in/motor = 4080 lbs

Table 2

Coefficient of friction (f)	
Steel on steel).5).8

To determine radial load capacity requirement of motor

When a motor used to drive a vehicle has the wheel or hub attached directly to the motor shaft, it is critical that the radial load capabilities of the motor are sufficient to support the vehicle. After calculating the Total Radial Load (RL) acting on the motors, the result must be compared to the bearing/shaft load charts for the chosen motor to determine if the motor will provide acceptable load capacity and life.

$$RL = \sqrt{W^2 + \left(\frac{T}{ri}\right)^2}$$
 lb $RL = \sqrt{W^2 + \left(\frac{T}{rm}\right)^2}$ kg

Example RL =
$$\sqrt{425^2 + \left(\frac{2936}{16}\right)^2} = 463 \text{ lbs}$$

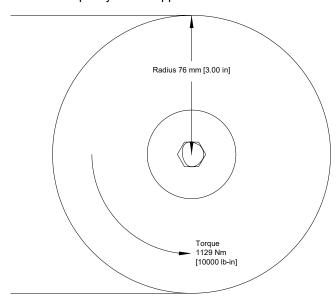
Once the maximum motor RPM, maximum torque requirement, and the maximum load each motor must support have been determined, these figures may then be compared to the motor performance charts and to the bearing load curves to choose a series and displacement to fulfill the motor requirements for the application.

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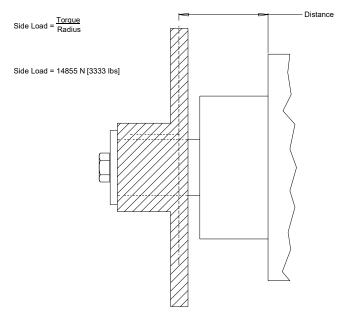


INDUCED SIDE LOAD

In many cases, pulleys or sprockets may be used to transmit the torque produced by the motor. Use of these components will create a torque induced side load on the motor shaft and bearings. It is important that this load be taken into consideration when choosing a motor with sufficient bearing and shaft capacity for the application.



To determine the side load, the motor torque and pulley or sprocket radius must be known. Side load may be calculated using the formula below. The distance from the pulley/sprocket centerline to the mounting flange of the motor must also be determined. These two figures may then be compared to the bearing and shaft load curve of the desired motor to determine if the side load falls within acceptable load ranges.



HYDRAULIC EQUATIONS

Multiplication Factor	Abbrev.	Prefix
10 ¹² 10 ⁹	T G	tera giga
10 ⁶	M	mega
10 ³	K	kilo
10 ²	h	hecto
10¹	da	deka
10 ⁻¹	d	deci
10 ⁻²	С	centi
10 ⁻³	m	milli
10-6	u	micro
10 ⁻⁹	n	nano
10 ⁻¹²	р	pico
10 ⁻¹⁵	f	femto
10 ⁻¹⁸	а	atto

Theo. Speed (RPM) =

1000 x LPM or 231 x GPM Displacement (cm³/rev) or Displacement (in³/rev)

Theo. Torque (lb-in) =

Power In (HP) =

Power Out (HP) =

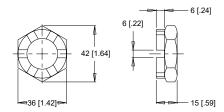


SHAFT NUT INFORMATION

35MM TAPERED SHAFTS

M24 x 1.5 Thread

A Slotted Nut



Torque Specifications: 32.5 daNm [240 ft.lb.]

PRECAUTION

The tightening torques listed with each nut should only be used as a guideline. Hubs may require higher or lower tightening torque depending on the material. Consult the hub manufacturer to obtain recommended tightening torque. To maximize torque transfer from the shaft to the hub, and to minimize the potential for shaft breakage, a hub with sufficient thickness must fully engage the taper length of the shaft.



incorrect



correct

12 [.47]

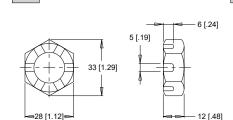
14 [.55]

1" TAPERED SHAFTS

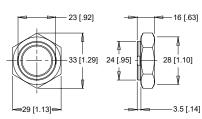
Slotted Nut

3/4-28 Thread

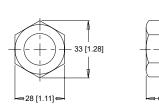
Α







C Solid Nut



Torque Specifications:

20 - 23 daNm [150 - 170 ft.lb.]

Torque Specifications: 24 - 27 daNm [180 - 200 ft.lb.]

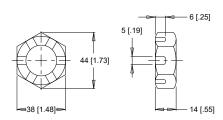
Torque Specifications:

20 - 23 daNm [150 - 170 ft.lb.]

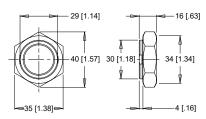
1-1/4" TAPERED SHAFTS

1-20 Thread

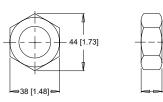




B Lock Nut



C Solid Nut



Torque Specifications:

38 daNm [280 ft.lb.] Max.

Torque Specifications: 33 - 42 daNm [240 - 310 ft.lb.]

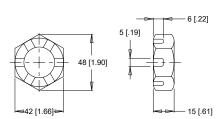
Torque Specifications: 38 daNm [280 ft.lb.] Max.

1-3/8" & 1-1/2" TAPERED SHAFTS

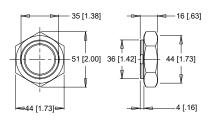
1 1/8-18 Thread

Slotted Nut

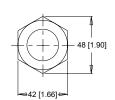
Α



B Lock Nut



C Solid Nut





Torque Specifications:

41 - 54 daNm [300 - 400 ft.lb.]

Torque Specifications:

34 - 48 daNm [250 - 350 ft.lb.]

Torque Specifications: 41

41 - 54 daNm [300 - 400 ft.lb.]



SPEED SENSORS

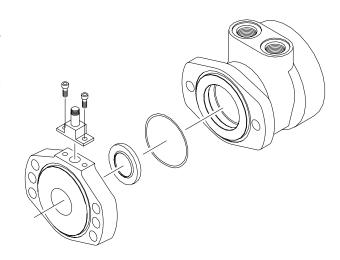
Impro Fluidtek offers both single and dual element speed sensor options providing a number of benefits to users by incorporating the latest advancements in sensing technology and materials. The single element sensors provide 50 pulses per revolution with the dual element providing 100 pulses per revolution." Higher resolution is especially beneficial for slow speed applications, where more information is needed for smooth and accurate control. The dual sensor option also provides a direction signal allowing end-users to monitor the direction of shaft rotation.

Unlike competitive designs that breach the high pressure area of the motor to add the sensor, the Impro Fluidtek speed sensor option utilizes an add-on flange to locate all sensor components outside the high pressure operating environment. This eliminates the potential leak point common to competitive designs. Many improvements were made to the sensor flange including changing the material from cast iron to acetal resin, incorporating a Buna-N shaft seal internal to the flange, and providing a grease zerk, which allows the user to fill the sensor cavity with grease. These improvements enable the flange to withstand the rigors of harsh environments.

Another important feature of the new sensor flange is that it is self-centering, which allows it to remain concentric to the magnet rotor. This produces a consistent mounting location for the new sensor module, eliminating the need to adjust

FEATURES / BENEFITS

- Grease fitting allows sensor cavity to be filled with grease for additional protection.
- Internal extruder seal protects against environmental elements.
- M12 or weatherpack connectors provide installation flexibility.
- Dual element sensor provides up to 100 pulses per revolution and directional sensing.
- Modular sensor allows quick and easy servicing.
- Acetal resin flange is resistant to moisture, chemicals, oils, solvents and greases.
- Self-centering design eliminates need to setmagnetto-sensor air gap.
- Protection circuitry



the air gap between the sensor and magnet rotor. The oring sealed sensor module attaches to the sensor flange with two small screws, allowing the sensor to be serviced or upgraded in the field in under one minute. This feature is especially valuable for mobile applications where machine downtime is costly. The sensor may also be serviced without exposing the hydraulic circuit to the atmosphere. Another advantage of the self-centering flange is that it allows users to rotate the sensor to a location best suited to their application. This feature is not available on competitive designs, which fix the sensor in one location in relationship to the motor mounting flange.

SENSOR OPTIONS

Z - 4-pin M12 male connector

This option has 50 pulses per revolution on all series. This option will not detect direction.

Y - 3-pin male weatherpack connector*

This option has 50 pulses per revolution on all series. This option will not detect direction.

X - 4-pin M12 male connector

This option has 100 pulses per revolution on all series. This option will detect direction.

W - 4-pin male weatherpack connector*

This option has 100 pulses per revolution on all series. This option will detect direction.

*These options include a 610mm [2 ft] cable.



SPEED SENSORS

SINGLE ELEMENT SENSOR - Y & Z

Supply voltages	7.5-24 Vdc
Maximum output off voltage	24 V
Maximum continuous output current	< 25 ma
Signal levels (low, high)	0.8 to supply voltage
Operating Temp30°C to 8	3°C [-22°F to 181°F]

DUAL ELEMENT SENSOR - X & W

Supply voltages	7.5-18 Vdc
Maximum output off voltage	18 V
Maximum continuous output current	< 20 ma
Signal levels (low, high)0.	8 to supply voltage
Operating Temp30°C to 83°C	C [-22°F to 181°F]

SENSOR CONNECTORS

Z Option

PIN



1	positive	brown or red		
2	n/a	white		
3	negative	blue		
4	pulse out	black		

X Option

PIN



1	positive	brown or red		
2	direction out	white		
3	negative	blue		
4	pulse out	black		

Y Option

PIN



Α	positive	brown or red			
В	negative	blue			
С	pulse out	black			
D	n/a	white			

W Option

PIN



Α	positive	brown or red		
В	negative	blue		
С	pulse out	black		
D	direction out	white		

PROTECTION CIRCUITRY

The single element sensor has been improved and incorporates protection circuitry to avoid electrical damage caused by:

- reverse battery protection
- overvoltage due to power supply spikes and surges (60 Vdc max.)
- · power applied to the output lead

The protection circuit feature will help "save" the sensor from damage mentioned above caused by:

- faulty installation wiring or system repair
- wiring harness shorts/opens due to equipment failure or harness damage resulting from accidental conditions (i.e. severed or grounded wire, ice, etc.)
- power supply spikes and surges caused by other electrical/electronic components that may be intermittent or damaged and "loading down" the system.

While no protection circuit can guarantee against any and all fault conditions. The single element sensor from Impro Fluidtek with protection circuitry is designed to handle potential hazards commonly seen in real world applications.

Unprotected versions are also available for operation at lower voltages down to 4.5V.

FREE TURNING ROTOR

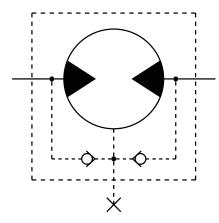
The 'AC' option or "Free turning" option refers to a specially prepared rotor assembly. This rotor assembly has increased clearance between the rotor tips and rollers allowing it to turn more freely than a standard rotor assembly. For spool valve motors, additional clearance is also provided between the shaft and housing bore. The 'AC' option is available for all motor series and displacements.

There are several applications and duty cycle conditions where 'AC' option performance characteristics can be beneficial. In continuous duty applications that require high flow/high RPM operation, the benefits are twofold. The additional clearance helps to minimize internal pressure drop at high flows. This clearance also provides a thicker oil film at metal to metal contact areas and can help extend the life of the motor in high RPM or even over speed conditions. The 'AC' option should be considered for applications that require continuous operation above 57 LPM [15 GPM] and/ or 300 RPM. Applications that are subject to pressure spikes due to frequent reversals or shock loads can also benefit by specifying the 'AC' option. The additional clearance serves to act as a buffer against spikes, allowing them to be bypassed through the motor rather than being absorbed and transmitted through the drive link to the output shaft. The trade-off for achieving these benefits is a slight loss of volumetric efficiency at high pressures.



INTERNAL DRAIN

The internal drain is standard on all WD, WP, WR, and WS360. Typically, a separate drain line must be installed to direct case leakage of the motor back to the reservoir when using, WS365/366. However, the internal drain option eliminates the need for a separate drain line through the installation of two check valves in the motor. This simplifies plumbing requirements for the motor.

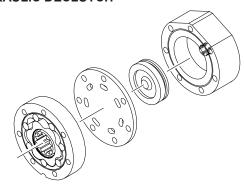


The two check valves connect the case area of the motor to each port of the endcover. During normal motor operation, pressure in the input and return lines of the motor close the check valves. However, when the pressure in the case of the motor is greater than that of the return line, the check valve between the case and low pressure line opens, allowing the case leakage to flow into the return line. Since the operation of the check valves is dependent upon a pressure differential, the internal drain option operates in either direction of motor rotation.

Although this option can simplify many motor installations, precautions must be taken to insure that return line pressure remains below allowable levels (see table below) to insure proper motor operation and life. If return line pressure is higher than allowable, or experiences pressure spikes, this pressure may feed back into the motor, possibly causing catastrophic seal failure. Installing motors with internal drains in series is not recommended unless overall pressure drop over all motors is below the maximum allowable backpressure as listed in the chart below. If in doubt, contact your authorized Impro Fluidtek representative.

MAXIMUM ALLOWABLE BACK PRESSURE								
Series	Cont. bar [psi]	Inter. bar [psi]						
WH	69 [1000]	103 [1500]						
WT	21 [300]	34 [500]						
Brakes	34 [500]	34 [500]						

HYDRAULIC DECLUTCH

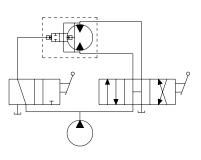


The declutch or 'AE' option, available on the RE and CE Series motors, has been specifically designed for applications requiring the motor to have the ability to "freewheel" when not pressurized. By making minor changes to internal components, the torque required to turn the output shaft is minimal. Selection of this option allows freewheeling speeds up to 1,000 RPM* depending on the displacement of the motor and duty cycle of the application.

To enable the motor to perform this function, the standard rotor assembly is replaced with a freeturn rotor assembly. Next, the standard balance plate and endcover is replaced with a special wear plate and ported endcover. The wear plate features seven holes that connect the stator pockets to each other. The ported endcover features a movable piston capable of sealing the seven holes in the wear plate.

When standard motor function is required, pressure is supplied to the endcover port, moving the piston against the wear plate. This action seals the seven holes allowing the motor to function as normal. However, when pressure is removed from the endcover port, the pressure created by the turning rotor assembly pushes the piston away from the wear plate, opening the rotor pockets to each other. In this condition, oil may circulate freely within the rotor and endcover assemblies, allowing the rotor assembly to rotate freely within the motor.

This option is especially useful in applications ranging from winch drives to towable wheel drives. Depending on the valves and hydraulic circuitry, operation of the freewheel function may be manually or automatically selected. A basic schematic is shown to the right.

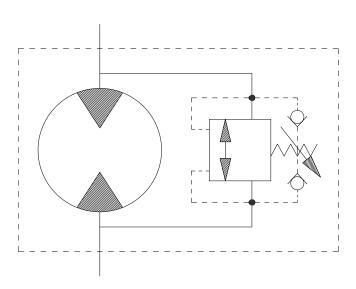


[▶] The 1,000 RPM rating was based on smaller displacement options with forced flow flushing through the motor to provide cooling.



VALVE CAVITY

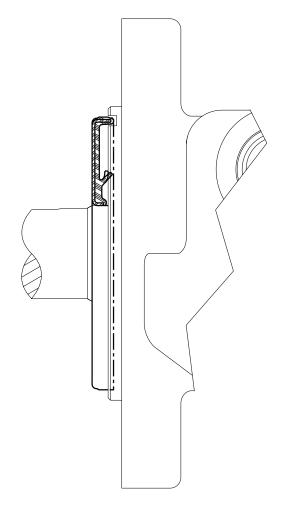
The valve cavity option provides a cost effective way to incorporate a variety of cartridge valves integral to the motor. The valve cavity is a standard 10 series 2-way cavity that accepts numerous cartridge valves, including overrunning check valves, relief cartridges, flow control valves, pilot operated check fuses, and high pressure shuttle valves. Installation of a relief cartridge into the cavity provides an extra margin of safety for applications encountering frequent pressure spikes. Relief cartridges from 69 to 207 bar [1000 to 3000 psi] may also be factory installed.



For basic systems with fixed displacement pumps, either manual or motorized flow control valves may be installed into the valve cavity to provide a simple method for controlling motor speed. It is also possible to incorporate the speed sensor option and a programmable logic controller with a motorized flow control valve to create a closed loop, fully automated speed control system. For motors with internal brakes, a shuttle valve cartridge may be installed into the cavity to provide a simple, fully integrated method for supplying release pressure to the pilot line to actuate an integral brake. To discuss other alternatives for the valve cavity option, contact an authorized Impro Fluidtek distributor.

SLINGER SEAL

Slinger seals are available on select series offered by Impro Fluidtek. Slinger seals offer extended shaft/shaft seal protection by prevented a buildup of material around the circumference of the shaft which can lead to premature shaft seal failures. The Impro Fluidtek slinger seals are designed to be larger in diameter than competitive products, providing greater surface speed and 'slinging action'.



Slinger seals are also available on 4-hole flange mounts on select series. Contact a Impro Fluidtek Customer Service Representative for additional information.

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For Medium Duty Applications

Impro Fluidtek

OVERVIEW

The WH Series motor features a case drain design, making it an ideal choice for medium-duty applications with high duty cycles or frequent direction reversals. This design offers several advantages, such as lowering pressure on the shaft seal and facilitating a cooling loop for the system. Additionally, the case flow helps lubricate essential drive components, enhancing motor longevity. An internal drain option is also available. The motor incorporates a laminated manifold and a three-zone orbiting valve, resulting in improved overall efficiency and greater usable power. Furthermore, a steel-faced seal in the orbiting valve minimizes the risk of seal extrusion or melting, which can occur in competing models.

FEATURES / BENEFITS

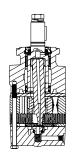
- Three bearing options available, enabling the load-carrying capabilities of the motor to be tailored to specific applications.
- The heavy-duty drive link stands out as the most robust in its category, featuring case flow lubrication that minimizes wear and extends its lifespan.
- Three-zone orbiting valve accurately controls oil flow, delivering outstanding volumetric efficiency.
- The rubber-energized steel face seal is designed to withstand high pressure and temperature without extruding or melting.
- Standard case drain allows reduced pressure on the shaft seal while maintaining driveline lubrication for maximum motor life.

TYPICAL APPLICATIONS

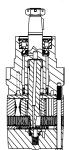
Medium-duty wheel drives, augers, mixers, winch drives, swing drives, grapple heads, feed rollers, broom drives, chippers, mining equipment, forrestry equipment and more

SERIES DESCRIPTIONS

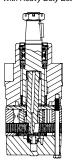
600 - Hydraulic Motor Standard



620 - Hydraulic Motor
With Medium Duty Bearin



630 - Hydraulic Motor
With Heavy Duty Bearing



SPECIFICATIONS

CODE	Displacement cm ³ [in ³ /rev]				Flow [gpm]	Max. Torque Nm [lb-in]		Max. Pressure bar [psi]		
	Citis [iiis/iev]	cont.	inter.	cont.	inter.	cont.	inter.	cont.	inter.	peak
200	204 [12.4]	465	558	95 [25]	114 [30]	558 [4936]	653 [5778]	207 [3000]	241 [3500]	276 [4000]
260	261 [15.9]	362	434	95 [25]	114 [30]	746 [6598]	868 [7677]	207 [3000]	241 [3500]	276 [4000]
300	300 [18.3]	315	378	95 [25]	114 [30]	846 [7485]	978 [8637]	207 [3000]	241 [3500]	276 [4000]
350	348 [21.2]	272	326	95 [25]	114 [30]	1018 [9010]	1172 [10367]	207 [3000]	241 [3500]	276 [4000]
375	375 [22.8]	253	303	95 [25]	114 [30]	1088 [9628]	1246 [11029]	207 [3000]	241 [3500]	276 [4000]
470	465 [28.3]	204	244	95 [25]	114 [30]	1142 [10106]	1362 [12056]	173 [2500]	207 [3000]	241 [3500]
540	536 [32.7]	176	211	95 [25]	114 [30]	1038 [9188]	1280 [11325]	138 [2000]	173 [2500]	207 [3000]
750	748 [45.6]	126	151	95 [25]	114 [30]	1040 [9207]	1399 [12382]	103 [1500]	138 [2000]	172 [2500]

[▶] Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing. Running at intermittent ratings should not exceed 10% of every minute of operation.



22.1 [.872]

mm [in]

72 [633]

DISPLACEMENT PERFORMANCE

פוט	PLAC		ENI PEI	KFUKIVI	ANCE								
			Pressure - ba	r [psi]		I	I	Γ	Max. Cont.	Max. Inter.	ı		
	200		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
	204 cm ³ [12	2.4 in ³]		[lb-in], Speed	rnm				Intermitte	nt Ratings - 1	0% of C	peration	
[md	2 [0.5]		38 [335]	77 [683]	.p						ΙГ	10	<u>ا</u>
Flow - Ipm [gpm]	4 [1]		39 [342]	85 [748]	174 [1543]	258 [2284]	329 [2913]					19	neoretical
y - Ic	8 [2]		38 [339]	90 [795]	13 178 [1579]	9 271 [2396]	5 361 [3192]	454 [4016]	519 [4594]	562 [4977]		38	cal rpm
FE	15 [4]		35 36 [323]	34 85 [749]	32 178 [1576]	28 283 [2506]	23 378 [3346]	16 459 [4059]	555 [4909]	3 636 [5625]		75	3
	23 [6]		73	72 78 [690]	69 177 [1562]	273 [2413]	57 362 [3202]	54 462 [4085]	44 551 [4880]	35 645 [5711]		112	
	30 [8]			74 [654]	106 172 [1518]	101 268 [2368]	97 357 [3156]	89 469 [4154]	80 558 [4936]	70 653 [5778]		150	
	38 [10]			148	145 168 [1491]	141 260 [2301]	133 349 [3091]	126 444 [3933]	117 541 [4783]	105 638 [5646]		187	
	45 [12]				184 156 [1381]	178 255 [2256]	174 350 [3096]	167 450 [3985]	156 542 [4793]	144 634 [5607]		224	
					221 150 [1332]	215 251 [2219]	209 330 [2919]	204 435 [3850]	199 526 [4653]	179 638 [5643]		261	
	53 [14]				259 133 [1180]	254 241 [2129]	250 336 [2970]	241 430 [3803]	231 522 [4616]	213 613 [5423]		299	
	61 [16]				297 122 [1082]	293 227 [2012]	286 328 [2899]	278 417 [3692]	276 510 [4510]	256 602 [5329]			
	68 [18]				335 112 [993]	332 214 [1897]	325 309 [2732]	319 401 [3547]	310 496 [4391]	298 587 [5198]		336	
	76 [20]				372	371 199 [1757]	365 303 [2680]	356 384 [3401]	348 493 [4358]	337 579 [5121]		373	
	83 [22]					409 184 [1625]	404 285 [2526]	396 380 [3366]	384 474 [4192]	374 562 [4970]	-	410	
r. r.	91 [24]					447 166 [1472]	443 277 [2453]	433 367 [3244]	423 463 [4101]	417 560 [4953]		448	
x. Max. er. Cont	95 [25]					465	461 219 [1935]	454 332 [2934]	443	432		466	
Max. Inter.	114 [30]						558	553			ı L	559	ı
	Rotor Width			iency - 70 - orque - Nm [lb		40 - 69%	0 - 39%						
	17.3			112 [987]	223 [1975]	335 [2962]	446 [3949]	558 [4936]	669 [5924]	794 [6044]	1		
	[.682] mm [in]		56 [494]	t tested at 54°					009 [3924]	781 [6911]	I		
	[]		Pressure - ba		O [123 1] Will	Tall oil viscos	sity of 4000t [2	.10 000]	Max. Cont.	Max. Inter.			
	260		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]	ĺ		
	261 cm ³ [15	5.9 in ³]	/ rev						Intermitte	nt Ratings - 1	0% of C	neration	
드			Torque - Nm 47 [417]	[lb-in], Speed 109 [962]	rpm				Intermitte	it itatings - i	олого I Г		1 –
Flow - Ipm [gpm]	2 [0.5]		5 51 [454]	110 [972]	238 [2104]	355 [3139]	460 [4074]					8	neoretical
v - Ipn	4 [1]		13 52 [462]	113 [1004]	11 242 [2145]	8 367 [3244]	5 485 [4292]	603 [5334]	715 [6323]			15	
Flov	8 [2]		28 49 [430]	27 111 [985]	25 239 [2115]	367 [3247] 367 [3247]	18 491 [4343]	14 619 [5474]	716 [6525] 11 746 [6598]	859 [7600]		30	-pm
	15 [4]		57	56	54	51	45	41	36	30		59	
	23 [6]		44 [391] 87	107 [950] 86	234 [2067] 83	364 [3225] 78	487 [4311] 72	617 [5458] 67	738 [6530] 60	854 [7557] 54		88	
	30 [8]			100 [884] 115	228 [2016] 113	355 [3146] 107	478 [4230] 103	612 [5418] 95	733 [6487] 89 734 [6498]	868 [7677] 82		117	
	38 [10]			90 [797] 145	220 [1947] 143	348 [3080] 138	468 [4143] 132	605 [5351] 123	115	852 [7541] 107		146	
	45 [12]			84 [748] 174	212 [1877] 172	340 [3011] 168	463 [4094] 162	596 [5272] 152	722 [6390] 143	845 [7481] 133		175	
	53 [14]			71 [631] 203	205 [1813] 201	330 [2921] 198	452 [4004] 185	587 [5195] 179	706 [6244] 173	846 [7491] 163		204	
	61 [16]				191 [1688] 231	317 [2807] 228	444 [3927] 223	574 [5077] 214	703 [6221] 203	824 [7291] 196		233	
	68 [18]				174 [1540] 261	305 [2698] 256	429 [3798] 251	560 [4952] 246	690 [6111] 230	815 [7214] 220		262	
	76 [20]				156 [1383] 290	289 [2558] 289	418 [3700] 282	544 [4817] 268	675 [5977] 262	810 [7166] 247		291	
	83 [22]				143 [1270] 319	275 [2431] 317	405 [3585] 313	533 [4717] 300	659 [5828] 293	787 [6961] 277		320	
	91 [24]				131 [1158] 348	255 [2253] 346	387 [3421] 342	515 [4554] 333	613 [5421] 322	769 [6805] 311		349	
Max. Cont.	95 [25]					239 [2115] 362	373 [3301] 357	505 [4471] 348	628 [5559] 342	772 [6832] 328		364	
Max. Max. Inter. Cont.	114 [30]					157 [1388] 434	298 [2637] 432	426 [3768] 427				436	
	Rotor		Overall Effic	iency - 70 -	100%	40 - 69%	0 - 39%					▶ P	er'
1	Width		Theoretical To	orque - Nm [lb	-in]	_			1		1		of p

143 [1266] 286 [2532] 429 [3798] 572 [5064]

Displacement tested at 54°C [129°F] with an oil viscosity of 46cSt [213 SUS]

▶ Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.

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715 [6330] 858 [7596]

1001 [8861]



DISPLACEMENT PERFORMANCE

סוס	PLAC	EIVIEN I PEI		ANCE				Man Cant	Man lates		
	200	Pressure - ba	T .	60 [1000]	104 [1500]	139 [3000]	172 [2500]	Max. Cont.	Max. Inter.		
	300 300 cm ³ [18	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]		
	300 cm [10	Torque - Nm	[lb-in], Speed	rpm				Intermitter	nt Ratings - 10	% of Operation	1
Flow - Ipm [gpm]	2 [0.5]	58 [509] 5	4	253 [2236] 4						7	Theor
<u>ud</u>	4 [1]	58 [517] 12	122 [1081] 11	266 [2353] 11	384 [3396] 11	509 [4501] 9	633 [5599] 9			13	Theoretical
. wol	8 [2]	58 [516] 25	128 [1134] 24	267 [2360] 24	404 3572] 23	553 [4893] 22	683 [6045] 21	813 [7198] 20	917 [8112] 20	26	Грт
_	15 [4]	56 [491] 50	132 [1173] 49	274 [2425] 49	417 [3691] 48	553 [4890] 47	703 [6225] 44	836 [7397] 43	962 [8513] 42	51	
	23 [6]	53 [466] 75	123 [1092] 75	269 [2384] 74	406 [3590] 73	559 [4949] 71	701 [6207] 69	831 [7356] 66	954 [8445] 63	76	
	30 [8]	44 [386] 100	117 [1036] 99	256 [2263] 97	419 [3710] 96	548 [4847] 95		846 [7485] 88		101	
	38 [10]		107 [947] 126	251 [2222] 126	390 [3448] 125		691 [6119] 119	836 [7396] 113		127	
	45 [12]		95 [841] 151	238 [2108] 150	400 [3538] 150	529 [4685] 149	696 [6160] 144	833 [7371] 140	969 [8573] 135	152	
	53 [14]		84 [748] 176	232 [2053] 175	366 [3237] 174			825 [7302] 164		177	
	61 [16]		71 [629] 201	217 [1920] 200	370 [3277] 198	508 [4494] 197		803 [7104] 187		202	
	68 [18]		201	202 [1792] 227	339 [2996] 226	503 [4448] 226		781 [6914] 214		228	
	76 [20]				326 [2887]	467 [4129] 249		772 [6831]		253	
	83 [22]			164 [1449]	251 308 [2726]	446 [3943]	604 [5346]		896 [7926]	278	
	91 [24]			147 [1304]	275 286 [2535]	274 437 [3871]				303	
ax.	95 [25]			302 116 [1024]			296 575 [5085]		285 848 [7500]	316	
Max. Max. Inter. Cont.	114 [30]			315	314 204 [1805]			309	302	379	-
⋝⊆	[]	Overall Effic	iency - 70 -	100%	378 40 - 69%	376 0 - 39%	370				J
	Rotor Width		orque - Nm [lb		40 - 03 %	_ 0 00%	′ 🔲				
	25.4 [1.000]	82 [729]	165 [1457]	329 [2914]	494 [4371]	659 [5828]	823 [7285]	988 [8742]	1152 [10199]		
	mm [in]	Displacemen	t tested at 54°	C [129°F] with	h an oil viscos	ity of 46cSt [2	213 SUS]				
		Pressure - ba	ar [psi]					Max. Cont.	Max. Inter.		
	350	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]		
	348 cm ³ [21		[lb-in], Speed	rpm				Intermitter	nt Ratings - 10	% of Operation	1
gpm]	2 [0.5]	69 [606] 4	140 [1243] 3	262 [2318] 2						6	Theo
Jud	4 [1]	75 [660] 10	153 [1350] 9	309 [2733] 7	454 [4014] 6					11	Theoretical
Flow - Ipm [gpm	8 [2]	75 [667] 21	158 [1395] 20	325 [2880] 17	489 [4326] 16	647 [5727] 14	784 [6937] 13	917 [8119] 11		22	l pm
ш.	15 [4]	73 [648] 43	159 [1405] 42	333 [2943] 38	502 [4443] 36	677 [5988] 33			1123 [9935] 26	44	
	23 [6]	67 [594] 65	152 [1346] 63		502 [4439] 55		841 [7444] 49			66	
	30 [8]	56 [494] 87	143 [1268] 85	317 [2808] 83	494 [4368] 78		833 [7376] 67			88	
	38 [10]	<u> </u>					830 [7345] 88			109	
	45 [12]		121 [1068] 130	291 [2578] 128	465 [4113] 122		817 [7231] 107		1169 [10342] 100	131	
	53 [14]		103 [907] 151	275 [2437] 148			815 [7212] 130		1162 [10284] 115	153	
	61 [16]		85 [755] 174		431 [3818] 168		790 [6991] 152		1141 [10099] 136	175	
	68 [18]		66 [587] 196		432 [3823] 190		768 [6800] 171		1131 [10012] 159	197	
	76 [20]		100	223 [1969] 217	391 [3459] 211		750 [6637] 196		1101 [9742] 176	218	
	83 [22]				372 [3293]		724 [6408] 219	909 [8049] 209		240	
	91 [24]			169 [1492] 261	236 349 [3085] 257	537 [4755] 253	698 [6179] 243	209	190	262	1
lax.	95 [25]			201	325 [2874]	507 [4491]	687 [6082]			273	1
Max. Max. Inter. Cont.	114 [30]				272 255 [2258]					327	1
≥ ⊆		Overall Effic	iency - 70 -	100%	40 - 69%	320 0 - 39%	315			L	Performance data is typical Performance
	Rotor Width		orque - Nm [lb		.0 00%					,	 Performance data is typical. Performance of production units varies slightly from one
	39.4 [1.553]	95 [844]	191 [1688]	381 [3376]	572 [5064]	763 [6752]	954 [8439]	1144 [10127]	1335 [11815]		motor to another. See page 6 for additional information on product testing.
	mm [in]	Displacemen	t tested at 54°	L C [129°F] with	h an oil viscos	ity of 46cSt [2	1213 SUS]	<u> </u>			. •



39.4 [1.553]

mm [in]

DISPLACEMENT PERFORMANCE

			Pressure - ba	ır [psi]					Max. Cont.	Max. Inter.	_		
	375		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
	375 cm ³ [22	 2.8 in³]	/ rev						Intermitte	I nt Ratings - 1] 0% of	Oneratio	n
딛			Torque - Nm 69 [611]	[lb-in], Speed	rpm				I	I Tutings - 1	0 70 O.]		_
Flow - Ipm [gpm]	2 [0.5]		74 [651]	161 [1425]	330 [2920]	494 [4369]	653 [5783]	823 [7283]				6	
/- lpn	4 [1]		74 [631] 9 76 [676]	173 [1527]	8 354 [3133]	7 518 [4582]	685 [6065]	5	1021 [9038]			11	
Flov	8 [2]		20	19	18	17 535 [4731]	15	13 883 [7814]	13 1032 [9130]	1101 [10541]		21	╝.
	15 [4]		73 [649] 40	158 [1399] 40	350 [3098] 38	37	706 [6250] 34 712 [6300]	32	30	1191 [10541] 30		41	4
	23 [6]		66 [588] 60	159 [1407] 60	346 [3058] 59	547 [4841] 57	54	49	1080 [9561] 47	1231 [10898] 45		61	4
	30 [8]		57 [502] 81	147 [1301] 80	337 [2980] 79	537 [4749] 77	700 [6192] 74	70	1088 [9628] 65	1236 [10941] 62		82	╛
	38 [10]			134 [1190] 101	323 [2856] 100	510 [4512] 99	694 [6139] 95	887 [7849] 90	1066 [9437] 85	1246 [11029] 79		102	
	45 [12]			124 [1097] 121	309 [2730] 120	496 [4385] 119	679 [6009] 114	883 [7817] 109	1073 [9493] 104	1244 [11010] 99		122	
	53 [14]			109 [961] 141	290 [2563] 140	477 [4217] 138	680 [6016] 136	130	1041 [9214] 123	1230 [10888] 117		142	
	61 [16]			82 [728] 162	267 [2362] 161	453 [4005] 159	637 [5641] 157	846 [7489] 150	144	1209 [10702] 136		163	
	68 [18]				248 [2198] 182	434 [3842] 180	619 [5474] 175	812 [7190] 171	1002 [8864] 165	1148 [10161] 162		183	
	76 [20]				229 [2026] 202	416 [3685] 201	600 [5309] 199	790 [6994] 192	979 [8664] 183	1145 [10137] 180		203	
	83 [22]				199 [1764] 222	385 [3406] 221	572 [5065] 219	761 [6738] 215	953 [8435] 210	1111 [9834] 201		223	7
	91 [24]				168 [1490] 243	362 [3204] 241	566 [5007] 240	731 [6471] 235				244	1
Max. Cont.	95 [25]					347 [3073] 253	554 [4905] 250	721 [6384] 245				254	7
Max. I Inter. (114 [30]					261 [2314] 303	440 [3891] 301	623 [5514] 300				304	7
	Rotor		Overall Effic	iency - 70 -	100%	40 - 69%	0 - 39%		•		•		_
	Width		Theoretical To	orque - Nm [lb	-in]	_					,		
	31.8 [1.252]		103 [908]	205 [1815]	410 [3631]	615 [5446]	821 [7261]	1026 [9076]	1231 [10892]	1436 [12707]			
	mm [in]		Displacement	t tested at 54°	C [129°F] witl	n an oil viscos	ity of 46cSt [2	213 SUS]			,		
			Pressure - ba	ır [psi]			I	Max. Cont.	Max. Inter.	1			
	470		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]				
	465 cm ³ [28	8.3 in ³]		[lb-in], Speed	rpm			Intermitte	nt Ratings - 1	0% of Operat	ion		
[mdf	2 [0.5]		92 [815] 3	195 [1723]	374 [3306]					5	The		
Flow - Ipm [gpm]	4 [1]		109 [967]	188 [1661]	418 [3701]	615 [5447] 4				9	Theoretical rpm		
- wo	8 [2]		99 [875]	217 [1924]	440 [3892]	668 [5910] 12	871 [7709]	1066 [9436]	1227 [10855]	17	= rpn		
Œ	15 [4]		93 [825]	213 [1887]	441 [3906]	688 [6086]			1343 [11886]	33	7		
	23 [6]		85 [751]	200 [1771]	29 434 [3841]	28 686 [6074]			18 1362 [12056]	49	1		
	30 [8]		72 [635]	186 [1645]	46 422 [3738]	659 [5834]			30 1352 [11963]	66			
	38 [10]		53 [472]	169 [1493]	404 [3579]	61 639 [5657]	58 874 [7734]	1115 [9871]	45 1351 [11958]	82			
	45 [12]		81	152 [1348]			74 855 [7563]		59 1340 [11861]	98			
	53 [14]			97 133 [1175]	96 364 [3221]	94 598 [5292]	89 833 [7374]		76 1319 [11673]	115			
	61 [16]			114 103 [910]	113 333 [2947]	112 569 [5037]	107 803 [7110]		90 1294 [11450]		\dashv		
	68 [18]			75 [661]	129 305 [2701]	128 555 [4908]	123 764 [6765]		104 1267 [11214]		\dashv		
	76 [20]			146	144 281 [2489]	143 507 [4490]	745 [6597]	133 985 [8719]	124 1236 [10940]	-	\dashv		
	83 [22]				163 227 [2011]	162 473 [4189]	156 714 [6322]	150 948 [8391]	141 1182 [10462]	-	\dashv		
					179 193 [1705]	178 432 [3827]	176 687 [6079]	168 915 [8093]	162	196	\dashv		
nt.	91 [24]				194	192 423 [3743]	191 651 [5759]	186 896 [7928]		l	\dashv		
ix. Max. er. Cont	95 [25]					204 321 [2840]	201 538 [4761]	191 784 [6938]		205	\dashv		
Max. Inter	114 [30]					244	242	238		245			
	Rotor			iency - 70 -		40 - 69%	0 - 39%					>	0 0
	Width		meoretical Id	orque - Nm [lb	-11]					,			m

127 [1127] | 255 [2253] | 509 [4506] | 764 [6760] | 1018 [9013] | 1273 [11266] 1528 [13519]

Displacement tested at 54°C [129°F] with an oil viscosity of 46cSt [213 SUS]

Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.

WH (All Series)

For Medium Duty Applications



DISPLACEMENT PERFORMANCE

DIS	PLAC		ERFORM	ANCE						
		Pressure				Max. Cont.	Max. Inter.			
	540	17 [250	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]			
	536 cm ³ [32	-	Nm [lb-in], Speed	rpm		Intermitter	nt Ratings - 10)% of	Operation	n
[mdf	2 [0.5]	108 [95:	3] 215 [1900] 2						4	Thec
Flow - Ipm [gpm]	4 [1]	107 [94	6] 225 [1995] 6	476 [4212] 5	710 [6284] 5	920 [8138] 3			8	heoretical
- wol	8 [2]	113 [996 13		498 [4403] 11	748 [6620] 11	980 [8674]	1220 [10798] 8		15	rpm
ш	15 [4]	115 [10 28		508 [4491] 26	779 [6893] 25	1038 [9188] 24	1266 [11201] 20		29	1
	23 [6]	102 [90:		505 [4465] 40	771 [6821] 38	1019 [9022] 36	1274 [11275] 32		43	1
	30 [8]	89 [79: 56		494 [4373] 55	764 [6759] 52	1020 [9029] 48	1280 [11325] 43		57	1
	38 [10]	71 [63 70		477 [4224] 68	750 [6639] 66	1016 [8994] 62	1277 [11299] 57		71	1
	45 [12]	47 [41 84		455 [4027] 84	729 [6455] 81	1001 [8858] 76	1288 [11394] 69		85	1
	53 [14]		158 [1397] 98	430 [3803] 97	702 [6214] 96	995 [8803] 89	1264 [11184] 82		99	1
	61 [16]		132 [1170] 113	403 [3564] 112	670 [5930] 110	944 [8353] 106	1240 [10970] 98		114	1
	68 [18]		97 [856] 127	366 [3236] 127	640 [5664] 126	935 [8276] 120	1193 [10557] 113		128	1
	76 [20]		63 [554] 141	335 [2962] 140	604 [6345] 139	878 [7767] 135	1156 [10228] 129		142	1
	83 [22]			303 [2680] 155	562 [4972] 153	838 [7420] 152	1115 [9868] 145		156	1
	91 [24]			242 [2141] 169	522 [4622] 167	813 [7194] 164	1075 [9517] 161		170	1
Max. Cont.	95 [25]			226 [1998] 176	490 [4338] 175	772 [6832] 174	1075 [9514] 165		177]
Max. Max. Inter. Cont.	114 [30]			98 [864] 211	380 [3365] 210	659 [5834] 209			212]
	Rotor	Overall E	fficiency - 70	- 100%	40 - 69%	0 - 39%				_
	Width	Theoretica	al Torque - Nm [li	o-in]						
	45.5 [1.791]	147 [130	294 [2604]	588 [5207]	883 [7811]	1177 [10414]	1471 [13018]			
	mm [in]		nent tested at 54	°C [129°F] with			13 SUS]			
	750	Pressure		60 [1000]	Max. Cont.	Max. Inter.				
		17 [250 5.6 in ³] / rev	35 [500]	69 [1000]	104 [1500]	138 [2000]				
		Torque - N	Nm [lb-in], Speed	rpm	Intermitte	nt Ratings - 1 ■	0% of Operati			
Flow - Ipm [gpm]	2 [0.5]	126 [11 ⁻	1	007 (5550)	000 10455		3	Theoretical rpm		
' - Iрп	4 [1]	156 [13] 4	3	627 [5552] 3	922 [8155] 2		6	tical		
Flow	8 [2]	153 [13: 9	9	664 [5873] 8	7	1308 [11579] 6	11	m		
	15 [4]	148 [13 20	19	686 [6071] 18	17	1374 [12161] 16	21	_		
	23 [6]	139 [12: 30	29	691 [6113] 28	27	1393 [12328] 25	31	_		
	30 [8]	123 [10] 40 99 [87]	40	681 [6026] 39	36	1380 [12211] 34	41	4		
	38 [10]	50 75 [66	49	48	47	1399 [12382] 45 1392 [12318]		4		
	45 [12]	60 46 [40	59	58 616 [5451]	57	55 1372 [12146]	61	4		
	53 [14]	70	70 190 [1682]	69 575 [5089]	68	64 1327 [11742]	71	4		
	61 [16]		81 150 [1325]	80 535 [4738]	78	76 1299 [11494]	82	4		
	68 [18]		91 107 [949]	90 486 [4298]	88	86 1253 [11090]	92	4		
	76 [20]		101	100 449 [3978]	100	97 1198 [10598]	102	4		
	83 [22]			111 384 [3401]	110 761 [6736]	108	112	4		
نے ن	91 [24]			121 369 [3268]	701 [0730] 120 737 [6523]	117	122	4		
Max. Max. Inter. Cont.	95 [25]			126 116 [1025]	125 494 [4374]	124	127	4		
Ma	114 [30]			151	149	<u> </u>	152	╛		
	Rotor Width		fficiency - 70 al Torque - Nm [ll		40 - 69%	0 - 39%				
	63.5	205 [181			1231 [10892	1641 [14522]				
	[2.501] mm [in]		nent tested at 54							
	[111]	Diopidoeii		- [0] WILL	110000	, 50001 [2				

▶ Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.



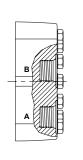
PORTING

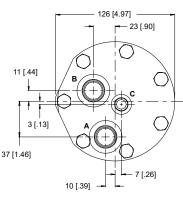
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

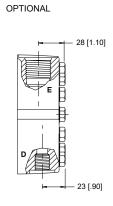
END PORTED - OFFSET

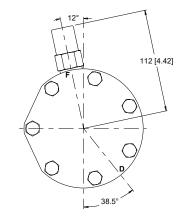
1 Main Ports **A**, **B**: 7/8-14 UNF
Drain Port **C**: 7/16-20 UNF

STANDARD









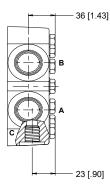
D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed

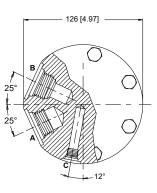
SIDE PORTED - RADIAL

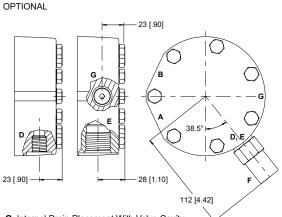
2 Main Ports **A, B**: G 3/4
Drain Port **C**: G 1/4

5 Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

STANDARD







D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity

WH (All Series)

For Medium Duty Applications



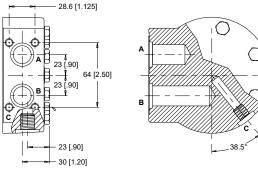
PORTING

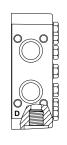
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

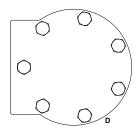
SIDE PORTED - MANIFOLD ALIGNED

Main Ports A, B: 11/16" Drilled
Drain Port C: 7/16-20 UNF

STANDARD OPTIONAL





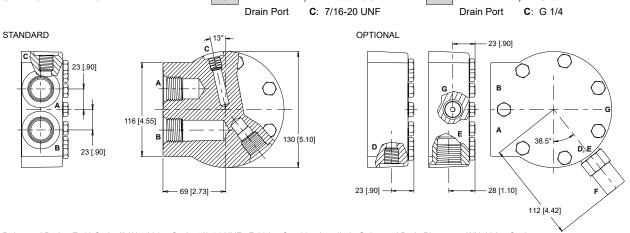


D: Internal Drain

SIDE PORTED - ALIGNED

6 Main Ports A, B: 1 1/16-20 UN

7 Main Ports A, B: G 3/4

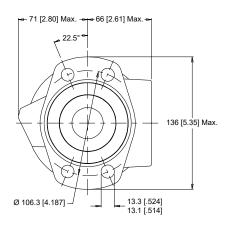


D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity

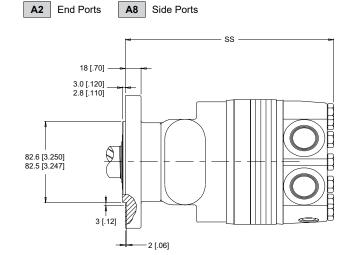


HOUSINGS

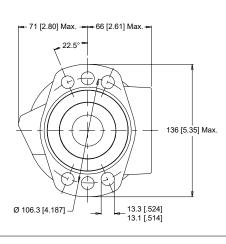
4-HOLE, MAGNETO MOUNT



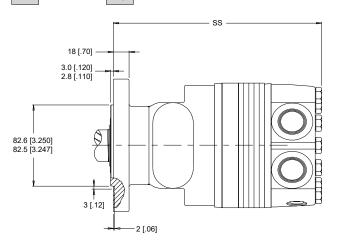
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].



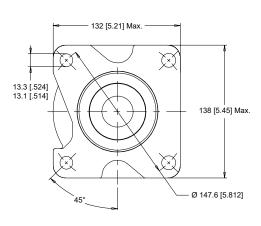
6-HOLE, SAE A MOUNT



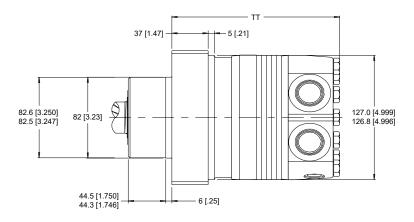




4-HOLE, WHEEL MOUNT



W2 End Ports W8 Side Ports



▶ Dimensions SS & TT are charted on page 24. Porting options listed on pages 21-22.

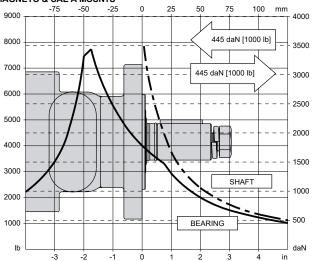


TECHNICAL INFORMATION

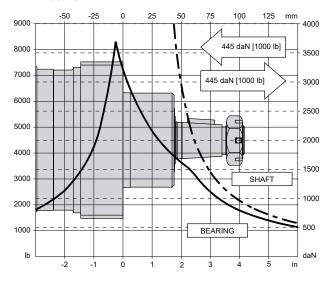
ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an L_{10} life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

MAGNETO & SAE A MOUNTS



WHEEL MOUNTS



LENGTH & WEIGHT CHART

Dimensions SS & TT are the overall motor lengths from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed on page 23.

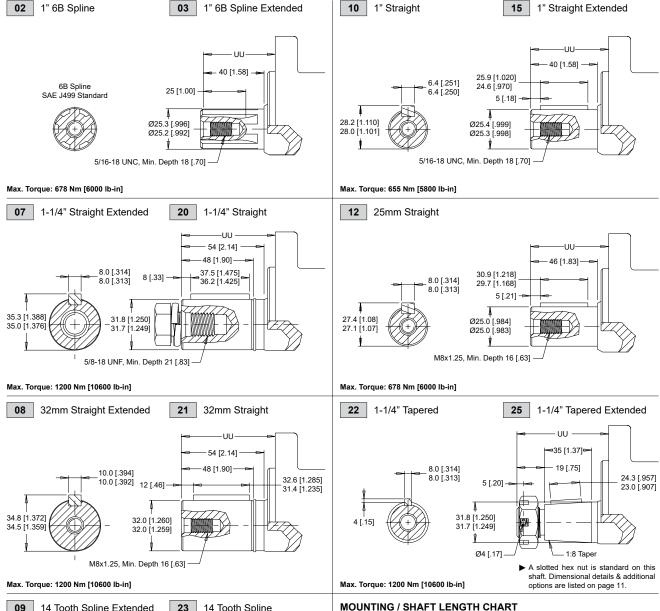
SS	Endcovers on pg. 21	Endcovers on pg. 22	Weight
#	mm [in]	mm [in]	kg [lb]
200	205 [8.08]	208 [8.19]	15.9 [35.0]
260	210 [8.26]	213 [8.37]	16.3 [36.0]
300	213 [8.39]	216 [8.50]	16.6 [36.6]
350	227 [8.95]	230 [9.06]	17.8 [39.2]
375	219 [8.75]	222 [8.75]	17.1 [37.8]
470	227 [8.95]	230 [9.06]	17.8 [39.2]
540	233 [9.18]	236 [9.29]	18.3 [40.3]
750	251 [9.89]	254 [10.00]	19.7 [43.5]

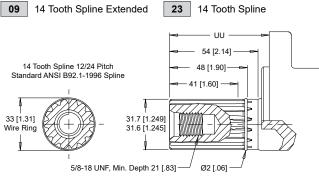
TT	Endcovers on pg. 21	Endcovers on pg. 22	Weight		
#	mm [in]	mm [in]	kg [lb]		
200	163 [6.42]	166 [6.53]	13.4 [29.6]		
260	168 [6.61]	171 [6.72]	13.9 [30.6]		
300	171 [6.74]	174 [6.85]	14.6 [32.2]		
350	185 [7.29]	188 [7.40]	15.7 [34.7]		
375	177 [6.99]	180 [7.10]	15.2 [33.4]		
470	185 [7.29]	188 [7.40]	15.7 [34.7]		
540	191 [7.53]	194 [7.64]	16.2 [35.8]		
750	209 [8.24]	212 [8.35]	17.7 [39.1]		

► All WH series motor weights can vary ± 0.9 kg [2 lb] depending on model configurations such as housing, shaft, endcover, options etc.



SHAFTS





Max. Torque: 1200 Nm [10600 lb-in]

Dimension UU is the overall distance from the motor mounting surface to the end of the shaft and is referenced on detailed shaft drawings above.

UU	Magneto & A Mounts	Wheel Mounts
#	mm [in]	mm [in]
02	50 [1.97]	91 [3.60]
03	76 [3.01]	118 [4.64]
07	88 [3.45]	129 [5.09]
08	88 [3.45]	129 [5.09]
09	88 [3.45]	129 [5.09]
10	50 [1.97]	91 [3.60]
12	56 [2.21]	98 [3.84]
15	76 [3.01]	118 [4.64]
20	61 [2.41]	103 [4.05]
21	61 [2.41]	103 [4.05]
22	66 [2.58]	107 [4.22]
23	61 [2.41]	103 [4.05]
25	92 [3.62]	134 [5.26]

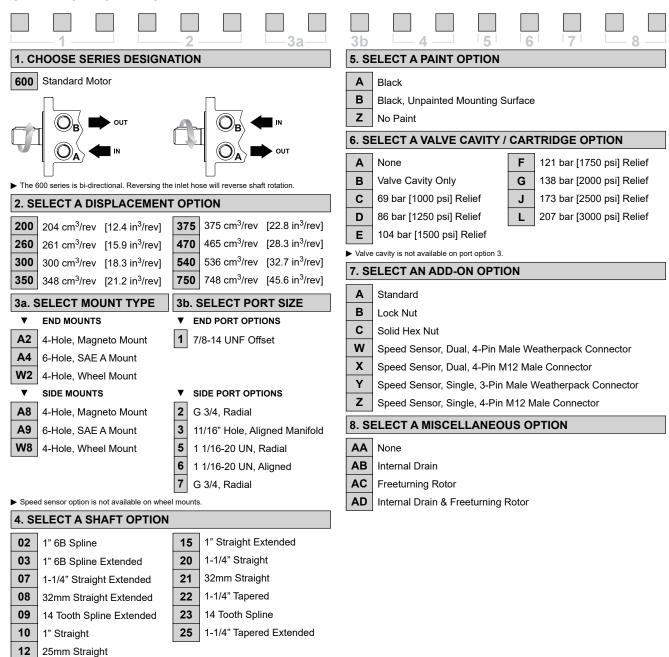
► Shaft lengths vary ± 0.8 mm [.030 in.]

WH (600 Series)

Medium Duty Hydraulic Motor



ORDERING INFORMATION



▶ For options not listed in the table above, please contact us with your requirements



HOUSINGS

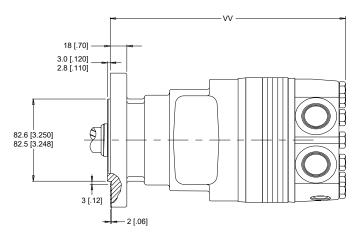
6-HOLE, SAE A MOUNT

13.3 [.524] 13.1 [.514] 0 106.3 [4.187]

▶ Porting options listed on pages 21-22.

▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].



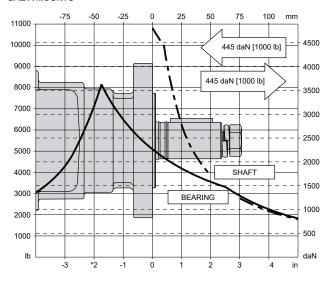


TECHNICAL INFORMATION

ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an L_{10} life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

SAE A MOUNTS



LENGTH & WEIGHT CHART

Dimension VV is the overall motor length from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed above.

➤ All WH series motor weights can vary ± 0.9 kg [2 lb] depending on model configurations such as housing, shaft, endcover, options etc.

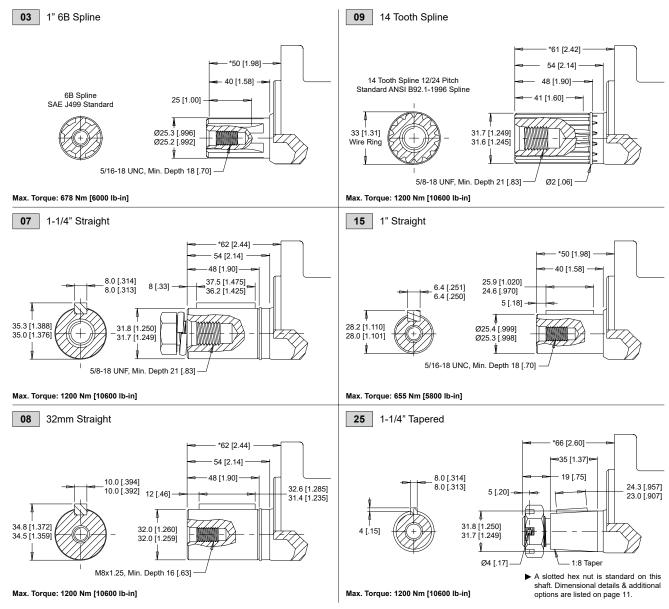
VV	Endcovers on pg. 21	Endcovers on pg. 22	Weight	
#	mm [in]	mm [in]	kg [lb]	
200	231 [9.08]	234 [9.19]	16.1 [35.4]	
260	235 [9.27]	238 [9.38]	16.2 [35.6]	
300	239 [9.40]	242 [9.51]	16.9 [37.2]	
350	253 [9.95]	256 [10.06]	18.0 [39.6]	
375	245 [9.65]	248 [9.76]	17.4 [38.3]	
470	253 [9.95]	256 [10.06]	18.0 [39.6]	
540	259 [10.19]	262 [10.30]	18.5 [40.7]	
750	277 [10.90]	280 [11.01]	20.0 [44.0]	

WH (620 Series)

Medium Duty Hydraulic Motor



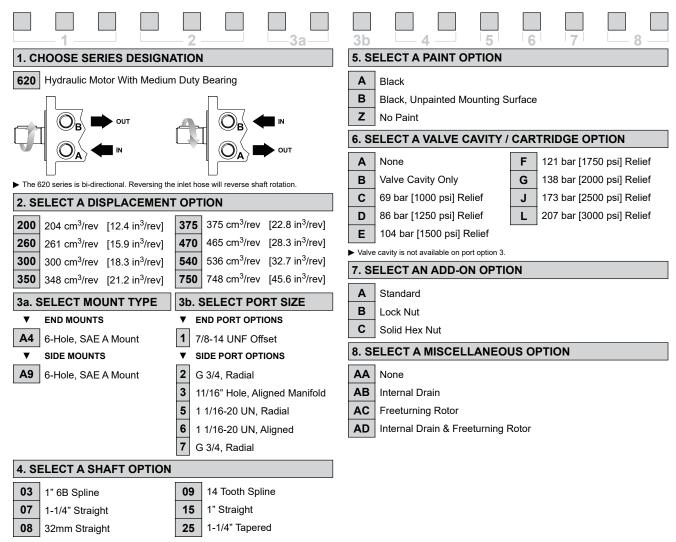
SHAFTS



▶ *Shaft lengths vary ± 0.8 mm [.030 in.]



ORDERING INFORMATION



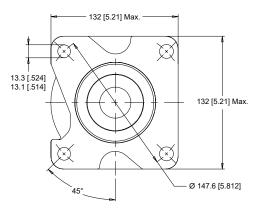
▶ For options not listed in the table above, please contact us with your requirements



127.0 [4.999] 126.8 [4.996]

HOUSINGS

4-HOLE, WHEEL MOUNT



▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

45.3 [1.785] 45.1 [1.775]

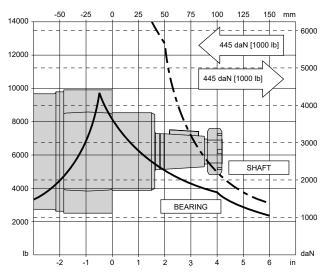
▶ Porting options listed on pages 21-20.

TECHNICAL INFORMATION

ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an L_{10} life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

WHEEL MOUNTS



LENGTH & WEIGHT CHART

82.6 [3.250]

82.5 [3.247]

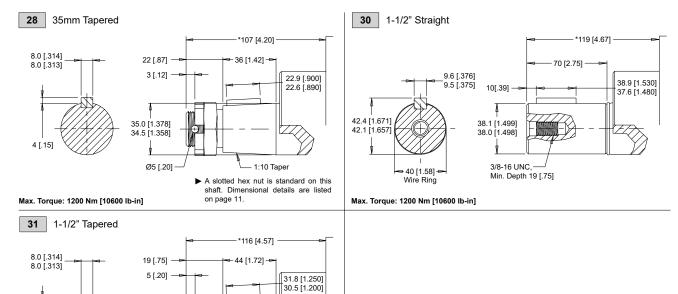
Dimension XX is the overall motor length from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed above.

► All WH series motor weights can vary ± 0.9
kg [2 lb] depending on model configurations
euch as housing shaft andcover ontions atc

XX	Endcovers on pg. 21	Endcovers on pg. 22		
#	mm [in]	mm [in]	kg [lb]	
200	199 [7.75]	202 [7.86]	17.5 [38.5]	
260	204 [8.04]	207 [8.15]	17.9 [39.5]	
300	207 [8.17]	210 [8.28]	18.2 [40.1]	
350	221 [8.72]	224 [8.83]	19.3 [42.6]	
375	214 [8.42]	217 [8.53]	18.7 [41.2]	
470	221 [8.72]	224 [8.83]	19.3 [42.6]	
540	227 [8.96]	230 [9.07]	19.8 [43.7]	
750	245 [9.67]	248 [9.78]	21.3 [47.0]	



SHAFTS



38.1 [1.500]
38.1 [1.499]

Ø4 [.17]

A slotted hex nut is standard on this

shaft. Dimensional details & additional options are listed on page 11.

Max. Torque: 1200 Nm [10600 lb-in]

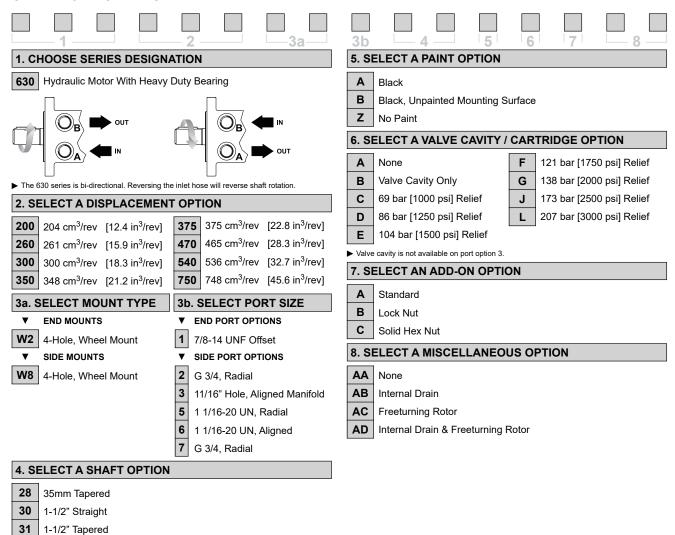
► *Shaft lengths vary ± 0.8 mm [.030 in.]

WH (630 Series)

Medium Duty Hydraulic Motor



ORDERING INFORMATION



▶ For options not listed in the table above, please contact us with your requirements



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