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#### OPERATING RECOMMENDATIONS

#### **OIL TYPE**

Hydraulic oils with anti-wear, anti-foam and demulsifiers are recommended for systems incorporating Impro Fluidtek motors. Straight oils can be used but may require VI (viscosity index) improvers depending on the operating temperature range of the system. Other water based and environmentally friendly oils may be used, but service life of the motor and other components in the system may be significantly shortened. Before using any type of fluid, consult the fluid requirements for all components in the system for compatibility. Testing under actual operating conditions is the only way to determine if acceptable service life will be achieved.

#### **FLUID VISCOSITY & FILTRATION**

Fluids with a viscosity between 20 - 43 cSt [100 - 200 S.U.S.] at operating temperature is recommended. Fluid temperature should also be maintained below 85°C [180° F]. It is also suggested that the type of pump and its operating specifications be taken into account when choosing a fluid for the system. Fluids with high viscosity can cause cavitation at the inlet side of the pump. Systems that operate over a wide range of temperatures may require viscosity improvers to provide acceptable fluid performance.

Impro Fluidtek recommends maintaining an oil cleanliness level of ISO 17-14 or better.

#### **INSTALLATION & START-UP**

When installing an Impro Fluidtek motor it is important that the mounting flange of the motor makes full contact with the mounting surface of the application. Mounting hardware of the appropriate grade and size must be used. Hubs, pulleys, sprockets and couplings must be properly aligned to avoid inducing excessive thrust or radial loads. Although the output device must fit the shaft snug, a hammer should never be used to install any type of output device onto the shaft. The port plugs should only be removed from the motor when the system connections are ready to be made. To avoid contamination, remove all matter from around the ports of the motor and the threads of the fittings. Once all system connections are made, it is recommended that the motor be run-in for 15-30 minutes at no load and half speed to remove air from the hydraulic system.

### MOTOR PROTECTION

Over-pressurization of a motor is one of the primary causes of motor failure. To prevent these situations, it is necessary to provide adequate relief protection for a motor based on the pressure ratings for that particular model. For systems that may experience overrunning conditions, special precautions must be taken. In an overrunning condition, the motor functions as a pump and attempts to convert kinetic energy into hydraulic energy. Unless the system is properly

configured for this condition, damage to the motor or system can occur. To protect against this condition a counterbalance valve or relief cartridge must be incorporated into the circuit to reduce the risk of over-pressurization. If a relief cartridge is used, it must be installed upline of the motor, if not in the motor, to relieve the pressure created by the over-running motor. To provide proper motor protection for an over-running load application, the pressure setting of the pressure relief valve must not exceed the intermittent rating of the motor.

#### HYDRAULIC MOTOR SAFETY PRECAUTION

A hydraulic motor must not be used to hold a suspended load. Due to the necessary internal tolerances, all hydraulic motors will experience some degree of creep when a load induced torque is applied to a motor at rest. All applications that require a load to be held must use some form of mechanical brake designed for that purpose.

#### MOTOR/BRAKE PRECAUTION

**Caution!** - Impro Fluidtek motor/brakes are intended to operate as static or parking brakes. System circuitry must be designed to bring the load to a stop before applying the brake.

Caution! - Because it is possible for some large displacement motors to overpower the brake, it is critical that the maximum system pressure be limited for these applications. Failure to do so could cause serious injury or death. When choosing a motor/brake for an application, consult the performance chart for the series and displacement chosen for the application to verify that the maximum operating pressure of the system will not allow the motor to produce more torque than the maximum rating of the brake. Also, it is vital that the system relief be set low enough to insure that the motor is not able to overpower the brake.

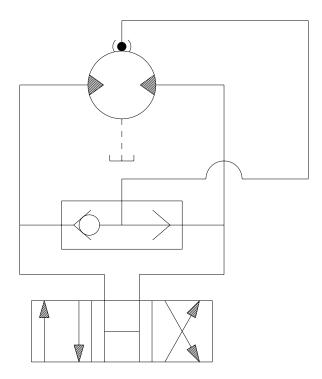
To ensure proper operation of the brake, a separate case drain back to tank must be used. Use of the internal drain option is not recommended due to the possibility of return line pressure spikes. A simple schematic of a system utilizing a motor/brake is shown on page 5. Although maximum brake release pressure may be used for an application, a 34 bar [500 psi] pressure reducing valve is recommended to promote maximum life for the brake release piston seals. However, if a pressure reducing valve is used in a system which has case drain back pressure, the pressure reducing valve should be set to 34 bar [500 psi] over the expected case pressure to ensure full brake release. To achieve proper brake release operation, it is necessary to bleed out any trapped air and fill brake release cavity and hoses before all connections are tightened. To facilitate this operation, all motor/brakes feature two release ports. One or both of these ports may be used to release the brake in the



# **OPERATING RECOMMENDATIONS & MOTOR CONNECTIONS**

#### MOTOR/BRAKE PRECAUTION

unit. Motor/brakes should be configured so that the release ports are near the top of the unit in the installed position.



Once all system connections are made, one release port must be opened to atmosphere and the brake release line carefully charged with fluid until all air is removed from the line and motor/brake release cavity. When this has been accomplished the port plug or secondary release line must be reinstalled. In the event of a pump or battery failure, an external pressure source may be connected to the brake release port to release the brake, allowing the machine to be moved.

▶ NOTE: It is vital that all operating recommendations be followed. Failure to do so could result in injury or death.

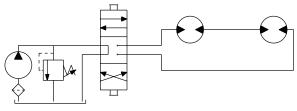
#### **MOTOR CIRCUITS**

There are two common types of circuits used for connecting multiple numbers of motors – series connection and parallel connection.

#### **SERIES CONNECTION**

When motors are connected in series, the outlet of one motor is connected to the inlet of the next motor. This allows the full pump flow to go through each motor and provide maximum speed. Pressure and torque are distributed between the motors based on the load each motor is

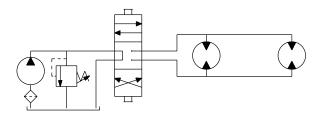
to. The maximum system pressure must be no greater than the maximum inlet pressure of the first motor. The allowable back pressure rating for a motor must also be considered. In some series circuits the motors must have an external case drain connected. A series connection is desirable when it is important for all the motors to run the same speed such as on a long line conveyor.



SERIES CIRCUIT

#### PARALLEL CONNECTION

In a parallel connection all of the motor inlets are connected. This makes the maximum system pressure available to each motor allowing each motor to produce full torque at that pressure. The pump flow is split between the individual motors according to their loads and displacements. If one motor has no load, the oil will take the path of least resistance and all the flow will go to that one motor. The others will not turn. If this condition can occur, a flow divider is recommended to distribute the oil and act as a differential.



PARALLEL CIRCUIT

▶ NOTE: The motor circuits shown above are for illustration purposes only. Components and circuitry for actual applications may vary greatly and should be chosen based on the application.



#### PRODUCT TESTING

Performance testing is the critical measure of a motor's ability to convert flow and pressure into speed and torque. All product testing is conducted using an Impro Fluidtek state of the art test facility. This facility utilizes fully automated test equipment and custom designed software to provide accurate, reliable test data. Test routines are standardized, including test stand calibration and stabilization of fluid temperature and viscosity, to provide consistent data. The example below provides an explanation of the values pertaining to each heading on the performance chart.

			Pressure - ba	rs [psi]					Max. Cont.	Max. Inter.			
	080		17 [250]	35 [500]	69 [1000]	104 [150	38 [2000]	173 [2500]	207 [3000]	242 [3500]			
76 (	cc [4.6 in <sup>3</sup> /r		rque - Nm [	lb-in], Speed	rpm				Intermitter	nt Ratings - 10	0% of C	Operation	ı
Flow - lpm [gpm]	2 [0.5]	(6	14 [127] <b>25</b>	30 [262] <b>24</b>	61 [543] <b>21</b>	91 [806] <b>18</b>	120 [1062] <b>17</b>	145 [1285] <b>11</b>	169 [1496] <b>11</b>	191 [1693] <b>9</b>	[	26	Theo
- Ipm	4 [1]		16 [140] <b>50</b>	32 [286] <b>50</b>	63 [559] <b>43</b>	95 [839] <b>43</b>	124 [1099] <b>34</b>	151 [1340] <b>32</b>	178 [1579] <b>32</b>	203 [1796] <b>31</b>	[	51	Theoretical rpm
-low	8 [2]		16 [139] <b>100</b>	32 [280] <b>100</b>	64 [563] <b>99</b>	97 [857] <b>92</b>	129 [1139] <b>87</b>	157 [1390] <b>79</b>	187 [1652] <b>78</b>	211 [1865] <b>77</b>		101	rpm
_	15 [4]		14 [127] <b>200</b>	31 [275] <b>200</b>	65 [572] <b>199</b>	99 [872] 191	131 [1155] <b>181</b>	160 [1420] <b>174</b>	186 [1643] <b>160</b>	216 [1911] <b>154</b>		201	
	23 [6]		13 [113] <b>301</b>	30 [262] <b>300</b>	63 [557] <b>297</b>	96 [853] <b>295</b>	130 [1149] <b>284</b>	160 [1420] <b>271</b>	186 [164 253	3 18 [1930] 245		302	
	1		10 [91] <b>401</b>	27 [243] <b>400</b>	61 [536] <b>398</b>	93 [826] <b>390</b>	127 [1125] <b>384</b>	159 [1409] <b>372</b>	187 [1654] <b>346</b>	220 [1945] <b>339</b>		4	
	38 [10]			24 [212] <b>502</b>	58 [511] <b>500</b>	89 [790] <b>499</b>	123 [1087] <b>498</b>	156 [1379] <b>485</b>	185 [1638] <b>443</b>	213 [1883] <b>433</b>		503	
	45 [12]			20 [177] <b>602</b>	54 [482] <b>601</b>	87 [767] <b>600</b>	120 [1060] <b>597</b>	164 [1451] <b>540</b>	193 [1711] <b>526</b>	228 [2021] <b>510</b>		603	
Max. Cont.	53 [14]			14 [127] <b>690</b>	50 [445] <b>689</b>	84 [741]	124 [1098] <b>658</b>	155 [1369] <b>644</b>	185 [1640] <b>631</b>	217 [1918] <b>613</b>	[	704	
	61 [16]											804	
Max. Inter.	64 [17]											904	
Overall Efficiency - 70 - 100% 40 - 69% 0 - 39%													
			Theoretical To	orque - Nm [lb	-in]								
			21 [183]	41 [366]	83 [732]	124 [109	66 [1465]	207 [1831]	248 [2197]	290 [2564]			
			Displacement	tested at 54°	C [129°F] with	an oil viscos	ity of 46cSt [2	13 SUS]					

- 1. Flow represents the amount of fluid passing through the motor during each minute of the test.
- Pressure refers to the measured pressure differential between the inlet and return ports of the motor during the test.
- The maximum continuous pressure rating and maximum intermittent pressure rating of the motor are separated by the dark lines on the chart.
- Theoretical RPM represents the RPM that the motor would produce if it were 100% volumetrically efficient. Measured RPM divided by the theoretical RPM give the actual volumetric efficiency of the motor.
- The maximum continuous flow rating and maximum intermittent flow rating of the motor are separated by the dark line on the chart.

- Performance numbers represent the actual torque and speed generated by the motor based on the corresponding input pressure and flow. The numbers on the top row indicate torque as measured in Nm [lb-in], while the bottom number represents the speed of the output shaft.
- 7. Areas within the white shading represent maximum motor efficiencies.
- 8. Theoretical Torque represents the torque that the motor would produce if it were 100% mechanically efficient. Actual torque divided by the theoretical torque gives the actual mechanical efficiency of the motor.



# **ALLOWABLE BEARING & SHAFT LOADING**

This catalog provides curves showing allowable radial loads at points along the longitudinal axis of the motor. They are dimensioned from the mounting flange. Two capacity curves for the shaft and bearings are shown. A vertical line through the centerline of the load drawn to intersect the x-axis intersects the curves at the load capacity of the shaft and of the bearing.

In the example below the maximum radial load bearing rating is between the internal roller bearings illustrated with a solid line. The allowable shaft rating is shown with a dotted line.

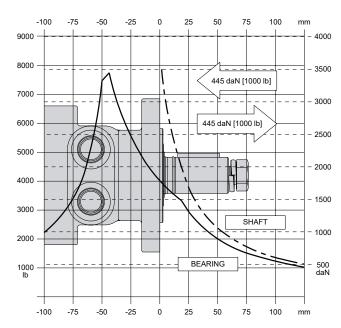
The bearing curves for each model are based on laboratory analysis and testing results constructed at Impro Fluidtek. The shaft loading is based on a 3:1 safety factor and 330 Kpsi tensile strength. The allowable load is the lower of the curves at a given point. For instance, one inch in front of the mounting flange the bearing capacity is lower than the shaft capacity. In this case, the bearing is the limiting load. The motor user needs to determine which series of motor to use based on their application knowledge.

#### ISO 281 RATINGS VS. MANUFACTURERS RATINGS

Published bearing curves can come from more than one type of analysis. The ISO 281 bearing rating is an international standard for the dynamic load rating of roller bearings. The rating is for a set load at a speed of 33 1/3 RPM for 500 hours (1 million revolutions). The standard was established to allow consistent comparisons of similar bearings between manufacturers. The ISO 281 bearing ratings are based solely on the physical characteristics of the bearings, removing any manufacturers specific safety factors or empirical data that influences the ratings.

Manufacturers' ratings are adjusted by diverse and systematic laboratory investigations, checked constantly with feedback from practical experience. Factors taken into account that affect bearing life are material, lubrication, cleanliness of the lubrication, speed, temperature, magnitude of the load and the bearing type.

The operating life of a bearing is the actual life achieved by the bearing and can be significantly different from the calculated life. Comparison with similar applications is the most accurate method for bearing life estimations.



# EXAMPLE LOAD RATING FOR MECHANICALLY RETAINED NEEDLE ROLLER BEARINGS

Bearing Life L <sub>10</sub> =	(C/P) <sup>p</sup> [10 <sup>s</sup> revolutions]
--------------------------------	--------------------------------------------------

L<sub>10</sub> = nominal rating life
C = dynamic load rating
P = equivalent dynamic load

Life Exponent p = 10/3 for needle bearings

BEARING LOAD MULTIPLICATION FACTOR TABLE				
RPM	FACTOR	RPM	FACTOR	
50	1.23	500	0.62	
100	1.00	600	0.58	
200	0.81	700	0.56	
300	0.72	800	0.50	
400	0.66			

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### **VEHICLE DRIVE CALCULATIONS**

When selecting a wheel drive motor for a mobile vehicle, a number of factors concerning the vehicle must be taken into consideration to determine the required maximum motor RPM, the maximum torque required and the maximum load each motor must support. The following sections contain the necessary equations to determine this criteria. An example is provided to illustrate the process.

# Sample application (vehicle design criteria)

vehicle description	4 wheel vehicle
vehicle drive	2 wheel drive
GVW	1,500 lbs.
weight over each drive wheel	425 lbs.
rolling radius of tires	16 in.
desired acceleration	
top speed	5 mph
gradability	20%
worst working surface	

### To determine maximum motor speed

DDM -	2.65 x KPH x G	RPM =	168 x MPH x G
RPM =	rm	KPIVI -	ri

Where:

MPH = max. vehicle speed (miles/hr)
KPH = max. vehicle speed (kilometers/hr)
ri = rolling radius of tire (inches)
G = gear reduction ratio (if none, G = 1)

rm = rolling radius of tire (meters)

**Example** RPM = 
$$\frac{168 \times 5 \times 1}{16}$$
 = 52.5

# To determine maximum torque requirement of motor

To choose a motor(s) capable of producing enough torque to propel the vehicle, it is necessary to determine the Total Tractive Effort (TE) requirement for the vehicle. To determine the total tractive effort, the following equation must be used:

# Where:

TE = Total tractive effort

RR = Force necessary to overcome rolling resistance

GR = Force required to climb a grade FA = Force required to accelerate

DP = Drawbar pull required

The components for this equation may be determined using the following steps:

# **Step One: Determine Rolling Resistance**

Rolling Resistance (RR) is the force necessary to propel a vehicle over a particular surface. It is recommended that the worst possible surface type to be encountered by the vehicle be factored into the equation.

$$RR = \frac{GVW}{1000} \times R \text{ (lb or N)}$$

Where:

GVW = gross (loaded) vehicle weight (lb or kg)
R = surface friction (value from Table1)

**Example** RR =  $\frac{1500}{1000}$  x 22 lbs = 33 lbs

Table 1

Rolling Resistance
Concrete (excellent)10
Concrete (good)15
Concrete (poor)20
Asphalt (good)12
Asphalt (fair)17
Asphalt (poor)22
Macadam (good)15
Macadam (fair)22
Macadam (poor)37
Cobbles (ordinary)55
Cobbles (poor)37
Snow (2 inch)25
Snow (4 inch)37
Dirt (smooth)25
Dirt (sandy)37
Mud37 to 150
Sand (soft)60 to 150
Sand (dune)160 to 300

# **Step Two: Determine Grade Resistance**

Grade Resistance (GR) is the amount of force necessary to move a vehicle up a hill or "grade." This calculation must be made using the maximum grade the vehicle will be expected to climb in normal operation.

To convert incline degrees to % Grade: % Grade = [tan of angle (degrees)] x 100

$$GR = \frac{\% \text{ Grade}}{100} \times GVW \text{ (lb or N)}$$

**Example** GR = 
$$\frac{20}{100}$$
 x 1500 lbs = 300 lbs



#### VEHICLE DRIVE CALCULATIONS

# **Step Three: Determine Acceleration Force**

Acceleration Force (FA) is the force necessary to accelerate from a stop to maximum speed in a desired time.

$$FA = \frac{MPH \times GVW \text{ (lb)}}{22 \times t} \qquad FA = \frac{KPH \times GVW \text{ (N)}}{35.32 \times t}$$

Where:

t = time to maximum speed (seconds)

**Example** FA = 
$$\frac{5 \times 1500 \text{ lbs}}{22 \times 10}$$
 = 34 lbs

# Step Four: Determine Drawbar Pull

Drawbar Pull (DP) is the additional force, if any, the vehicle will be required to generate if it is to be used to tow other equipment. If additional towing capacity is required for the equipment, repeat steps one through three for the towable equipment and sum the totals to determine DP.

#### **Step Five: Determine Total Tractive Effort**

The Tractive Effort (TE) is the sum of the forces calculated in steps one through three above. On low speed vehicles, wind resistance can typically be neglected. However, friction in drive components may warrant the addition of 10% to the total tractive effort to insure acceptable vehicle performance.

$$TE = RR + GR + FA + DP (lb or N)$$

**Example** TE = 
$$33 + 300 + 34 + 0$$
 (lbs) =  $367$  lbs

# Step Six: Determine Motor Torque

The Motor Torque (T) required per motor is the Total Tractive Effort divided by the number of motors used on the machine. Gear reduction is also factored into account in this equation.

$$T = \begin{array}{cc} \frac{TE \ x \ ri}{M \ x \ G} & \text{Ib-in per motor} & T = \frac{TE \ x \ rm}{M \ x \ G} & \text{Nm per motor} \end{array}$$

Where:

M = number of driving motors

**Example** 
$$T = \frac{367 \times 16}{2 \times 1}$$
 lb-in/motor = 2936 lb-in

# **Step Seven: Determine Wheel Slip**

To verify that the vehicle will perform as designed in regards to tractive effort and acceleration, it is necessary to calculate wheel slip (TS) for the vehicle. In special cases, wheel slip may actually be desirable to prevent hydraulic system overheating and component breakage should the vehicle become stalled.

$$TS = \frac{W \times f \times ri}{G}$$

$$TS = \frac{W \times f \times rm}{G}$$
(Ib-in per motor)
(N-m per motor)

Where:

f = coefficient of friction (see table 2)

W = loaded vehicle weight over driven wheel (lb or N)

**Example** TS = 
$$\frac{425 \times .06 \times 16}{1}$$
 lb-in/motor = 4080 lbs

Table 2

Coefficient of friction (f)	
Steel on steel	.5 .8

# To determine radial load capacity requirement of motor

When a motor used to drive a vehicle has the wheel or hub attached directly to the motor shaft, it is critical that the radial load capabilities of the motor are sufficient to support the vehicle. After calculating the Total Radial Load (RL) acting on the motors, the result must be compared to the bearing/shaft load charts for the chosen motor to determine if the motor will provide acceptable load capacity and life.

$$RL = \sqrt{W^2 + \left(\frac{T}{ri}\right)^2}$$
 lb  $RL = \sqrt{W^2 + \left(\frac{T}{rm}\right)^2}$  kg

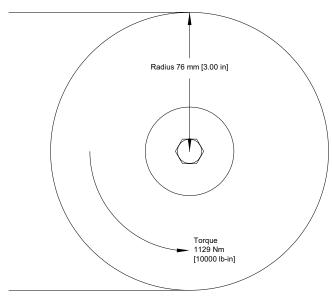
**Example** RL = 
$$\sqrt{425^2 + \left(\frac{2936}{16}\right)^2}$$
 = 463 lbs

Once the maximum motor RPM, maximum torque requirement, and the maximum load each motor must support have been determined, these figures may then be compared to the motor performance charts and to the bearing load curves to choose a series and displacement to fulfill the motor requirements for the application.

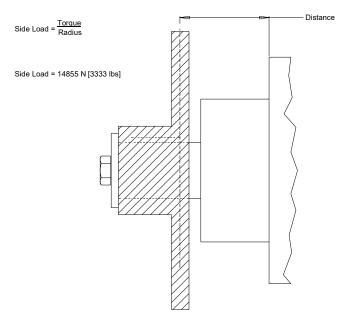


# **INDUCED SIDE LOAD**

In many cases, pulleys or sprockets may be used to transmit the torque produced by the motor. Use of these components will create a torque induced side load on the motor shaft and bearings. It is important that this load be taken into consideration when choosing a motor with sufficient bearing and shaft capacity for the application.



To determine the side load, the motor torque and pulley or sprocket radius must be known. Side load may be calculated using the formula below. The distance from the pulley/sprocket centerline to the mounting flange of the motor must also be determined. These two figures may then be compared to the bearing and shaft load curve of the desired motor to determine if the side load falls within acceptable load ranges.



# **HYDRAULIC EQUATIONS**

Multiplication Factor	Abbrev.	Prefix
10 <sup>12</sup>	Т	tera
10 <sup>9</sup>	G	giga
10 <sup>6</sup>	M	mega
10 <sup>3</sup>	K	kilo
10 <sup>2</sup>	h	hecto
10¹	da	deka
10 <sup>-1</sup>	d	deci
10-2	С	centi
10 <sup>-3</sup>	m	milli
10-6	u	micro
10 <sup>-9</sup>	n	nano
10 <sup>-12</sup>	р	pico
10 <sup>-15</sup>	f	femto
10 <sup>-18</sup>	а	atto

Theo. Speed (RPM) =

 $\frac{1000 \text{ x LPM}}{\text{Displacement (cm}^3/\text{rev})}$  or  $\frac{231 \text{ x GPM}}{\text{Displacement (in}^3/\text{rev})}$ 

Theo. Torque (lb-in) =

Bar x Disp. (cm³/rev)
20 pi

or PSI x Displacement (in³/rev)
6.28

Power In (HP) =

Bar x LPM or PSI x GPM 1714

Power Out (HP) =

<u>Torque (Nm) x RPM</u> 9543 or <u>Torque (lb-in) x RPM</u> 63024

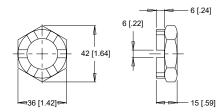


#### SHAFT NUT INFORMATION

#### 35MM TAPERED SHAFTS

M24 x 1.5 Thread

A Slotted Nut



Torque Specifications: 32.5 daNm [240 ft.lb.]

#### PRECAUTION

The tightening torques listed with each nut should only be used as a guideline. Hubs may require higher or lower tightening torque depending on the material. Consult the hub manufacturer to obtain recommended tightening torque. To maximize torque transfer from the shaft to the hub, and to minimize the potential for shaft breakage, a hub with sufficient thickness must fully engage the taper length of the shaft.



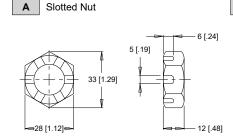
incorrect



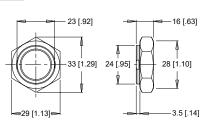
correct

# 1" TAPERED SHAFTS

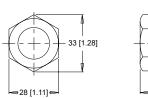
3/4-28 Thread







C Solid Nut





Torque Specifications:

20 - 23 daNm [150 - 170 ft.lb.]

Torque Specifications:

24 - 27 daNm [180 - 200 ft.lb.]

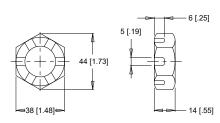
Torque Specifications:

20 - 23 daNm [150 - 170 ft.lb.]

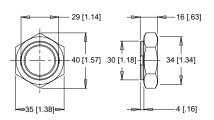
#### 1-1/4" TAPERED SHAFTS

1-20 Thread

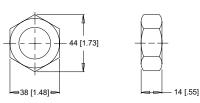




B Lock Nut



C Solid Nut



Torque Specifications:

38 daNm [280 ft.lb.] Max.

Torque Specifications: 33 - 42 daNm [240 - 310 ft.lb.]

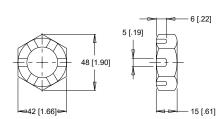
Torque Specifications: 38 daNm [280 ft.lb.] Max.

# 1-3/8" & 1-1/2" TAPERED SHAFTS

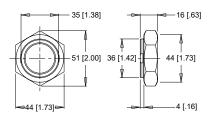
1 1/8-18 Thread

Slotted Nut

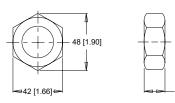
Α



B Lock Nut



C Solid Nut



Torque Specifications:

41 - 54 daNm [300 - 400 ft.lb.]

Torque Specifications:

34 - 48 daNm [250 - 350 ft.lb.]

Torque Specifications: 41 - 54 daNm [300 - 400 ft.lb.]

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15 [.61]



#### SPEED SENSORS

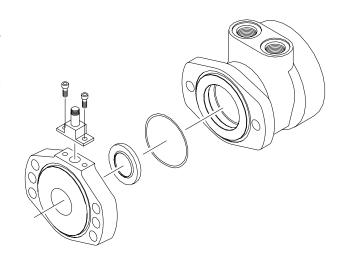
Impro Fluidtek offers both single and dual element speed sensor options providing a number of benefits to users by incorporating the latest advancements in sensing technology and materials. The single element sensors provide 50 pulses per revolution with the dual element providing 100 pulses per revolution." Higher resolution is especially beneficial for slow speed applications, where more information is needed for smooth and accurate control. The dual sensor option also provides a direction signal allowing end-users to monitor the direction of shaft rotation.

Unlike competitive designs that breach the high pressure area of the motor to add the sensor, the Impro Fluidtek speed sensor option utilizes an add-on flange to locate all sensor components outside the high pressure operating environment. This eliminates the potential leak point common to competitive designs. Many improvements were made to the sensor flange including changing the material from cast iron to acetal resin, incorporating a Buna-N shaft seal internal to the flange, and providing a grease zerk, which allows the user to fill the sensor cavity with grease. These improvements enable the flange to withstand the rigors of harsh environments.

Another important feature of the new sensor flange is that it is self-centering, which allows it to remain concentric to the magnet rotor. This produces a consistent mounting location for the new sensor module, eliminating the need to adjust

#### **FEATURES / BENEFITS**

- Grease fitting allows sensor cavity to be filled with grease for additional protection.
- Internal extruder seal protects against environmental elements.
- M12 or weatherpack connectors provide installation flexibility.
- Dual element sensor provides up to 100 pulses per revolution and directional sensing.
- Modular sensor allows quick and easy servicing.
- Acetal resin flange is resistant to moisture, chemicals, oils, solvents and greases.
- Self-centering design eliminates need to setmagnetto-sensor air gap.
- Protection circuitry



the air gap between the sensor and magnet rotor. The oring sealed sensor module attaches to the sensor flange with two small screws, allowing the sensor to be serviced or upgraded in the field in under one minute. This feature is especially valuable for mobile applications where machine downtime is costly. The sensor may also be serviced without exposing the hydraulic circuit to the atmosphere. Another advantage of the self-centering flange is that it allows users to rotate the sensor to a location best suited to their application. This feature is not available on competitive designs, which fix the sensor in one location in relationship to the motor mounting flange.

#### **SENSOR OPTIONS**

# Z - 4-pin M12 male connector

This option has 50 pulses per revolution on all series. This option will not detect direction.

### Y - 3-pin male weatherpack connector\*

This option has 50 pulses per revolution on all series. This option will not detect direction.

# X - 4-pin M12 male connector

This option has 100 pulses per revolution on all series. This option will detect direction.

# W - 4-pin male weatherpack connector\*

This option has 100 pulses per revolution on all series. This option will detect direction.

\*These options include a 610mm [2 ft] cable.



#### SPEED SENSORS

#### SINGLE ELEMENT SENSOR - Y & Z

Supply voltages	7.5-24 Vdc
Maximum output off voltage	24 V
Maximum continuous output current	< 25 ma
Signal levels (low, high) 0.8 to s	upply voltage
Operating Temp30°C to 83°C [-22	2°F to 181°F]

### **DUAL ELEMENT SENSOR - X & W**

Supply voltages	7.5-18 Vdc
Maximum output off voltage	18 V
Maximum continuous output current	< 20 ma
Signal levels (low, high) 0.8 to	supply voltage
Operating Temp30°C to 83°C [-2	22°F to 181°F]

#### SENSOR CONNECTORS

#### Z Option

#### PIN



1	positive	brown or red		
2	n/a	white		
3	negative	blue		
4	pulse out	black		

#### X Option

# PIN



1	positive	brown or red			
2	direction out	white			
3	negative	blue			
4	pulse out	black			

# Y Option

# PIN



Α	positive	brown or red			
В	negative	blue			
C	pulse out	black			
D	n/a	white			

#### W Option

# PIN



Α	positive	brown or red
В	negative	blue
С	pulse out	black
D	direction out	white

#### PROTECTION CIRCUITRY

The single element sensor has been improved and incorporates protection circuitry to avoid electrical damage caused by:

- reverse battery protection
- overvoltage due to power supply spikes and surges (60 Vdc max.)
- · power applied to the output lead

The protection circuit feature will help "save" the sensor from damage mentioned above caused by:

- faulty installation wiring or system repair
- wiring harness shorts/opens due to equipment failure or harness damage resulting from accidental conditions (i.e. severed or grounded wire, ice, etc.)
- power supply spikes and surges caused by other electrical/electronic components that may be intermittent or damaged and "loading down" the system.

While no protection circuit can guarantee against any and all fault conditions. The single element sensor from Impro Fluidtek with protection circuitry is designed to handle potential hazards commonly seen in real world applications.

Unprotected versions are also available for operation at lower voltages down to 4.5V.

#### FREE TURNING ROTOR

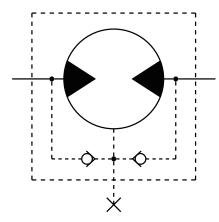
The 'AC' option or "Free turning" option refers to a specially prepared rotor assembly. This rotor assembly has increased clearance between the rotor tips and rollers allowing it to turn more freely than a standard rotor assembly. For spool valve motors, additional clearance is also provided between the shaft and housing bore. The 'AC' option is available for all motor series and displacements.

There are several applications and duty cycle conditions where 'AC' option performance characteristics can be beneficial. In continuous duty applications that require high flow/high RPM operation, the benefits are twofold. The additional clearance helps to minimize internal pressure drop at high flows. This clearance also provides a thicker oil film at metal to metal contact areas and can help extend the life of the motor in high RPM or even over speed conditions. The 'AC' option should be considered for applications that require continuous operation above 57 LPM [15 GPM] and/ or 300 RPM. Applications that are subject to pressure spikes due to frequent reversals or shock loads can also benefit by specifying the 'AC' option. The additional clearance serves to act as a buffer against spikes, allowing them to be bypassed through the motor rather than being absorbed and transmitted through the drive link to the output shaft. The trade-off for achieving these benefits is a slight loss of volumetric efficiency at high pressures.



#### **INTERNAL DRAIN**

The internal drain is standard on all WD, WP, WR, and WS360. Typically, a separate drain line must be installed to direct case leakage of the motor back to the reservoir when using, WS365/366. However, the internal drain option eliminates the need for a separate drain line through the installation of two check valves in the motor. This simplifies plumbing requirements for the motor.

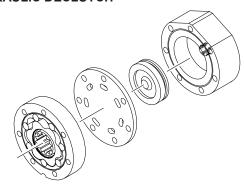


The two check valves connect the case area of the motor to each port of the endcover. During normal motor operation, pressure in the input and return lines of the motor close the check valves. However, when the pressure in the case of the motor is greater than that of the return line, the check valve between the case and low pressure line opens, allowing the case leakage to flow into the return line. Since the operation of the check valves is dependent upon a pressure differential, the internal drain option operates in either direction of motor rotation.

Although this option can simplify many motor installations, precautions must be taken to insure that return line pressure remains below allowable levels (see table below) to insure proper motor operation and life. If return line pressure is higher than allowable, or experiences pressure spikes, this pressure may feed back into the motor, possibly causing catastrophic seal failure. Installing motors with internal drains in series is not recommended unless overall pressure drop over all motors is below the maximum allowable backpressure as listed in the chart below. If in doubt, contact your authorized Impro Fluidtek representative.

MAXIMUM ALLOWABLE BACK PRESSURE								
Series	Cont. bar [psi]	Inter. bar [psi]						
WH	69 [1000]	103 [1500]						
WT	21 [300]	34 [500]						
Brakes	34 [500]	34 [500]						

#### HYDRAULIC DECLUTCH

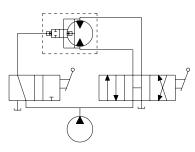


The declutch or 'AE' option, available on the RE and CE Series motors, has been specifically designed for applications requiring the motor to have the ability to "freewheel" when not pressurized. By making minor changes to internal components, the torque required to turn the output shaft is minimal. Selection of this option allows freewheeling speeds up to 1,000 RPM\* depending on the displacement of the motor and duty cycle of the application.

To enable the motor to perform this function, the standard rotor assembly is replaced with a freeturn rotor assembly. Next, the standard balance plate and endcover is replaced with a special wear plate and ported endcover. The wear plate features seven holes that connect the stator pockets to each other. The ported endcover features a movable piston capable of sealing the seven holes in the wear plate.

When standard motor function is required, pressure is supplied to the endcover port, moving the piston against the wear plate. This action seals the seven holes allowing the motor to function as normal. However, when pressure is removed from the endcover port, the pressure created by the turning rotor assembly pushes the piston away from the wear plate, opening the rotor pockets to each other. In this condition, oil may circulate freely within the rotor and endcover assemblies, allowing the rotor assembly to rotate freely within the motor.

This option is especially useful in applications ranging from winch drives to towable wheel drives. Depending on the valves and hydraulic circuitry, operation of the freewheel function may be manually or automatically selected. A basic schematic is shown to the right.

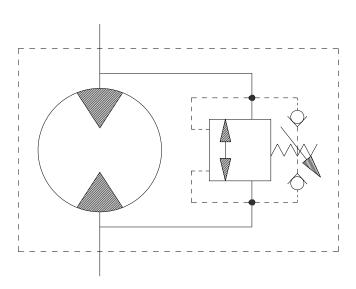


<sup>▶</sup> The 1,000 RPM rating was based on smaller displacement options with forced flow flushing through the motor to provide cooling.



# **VALVE CAVITY**

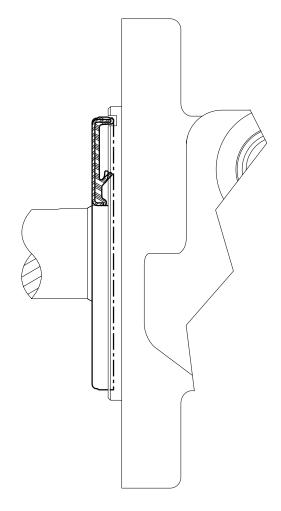
The valve cavity option provides a cost effective way to incorporate a variety of cartridge valves integral to the motor. The valve cavity is a standard 10 series 2-way cavity that accepts numerous cartridge valves, including overrunning check valves, relief cartridges, flow control valves, pilot operated check fuses, and high pressure shuttle valves. Installation of a relief cartridge into the cavity provides an extra margin of safety for applications encountering frequent pressure spikes. Relief cartridges from 69 to 207 bar [1000 to 3000 psi] may also be factory installed.



For basic systems with fixed displacement pumps, either manual or motorized flow control valves may be installed into the valve cavity to provide a simple method for controlling motor speed. It is also possible to incorporate the speed sensor option and a programmable logic controller with a motorized flow control valve to create a closed loop, fully automated speed control system. For motors with internal brakes, a shuttle valve cartridge may be installed into the cavity to provide a simple, fully integrated method for supplying release pressure to the pilot line to actuate an integral brake. To discuss other alternatives for the valve cavity option, contact an authorized Impro Fluidtek distributor.

#### SLINGER SEAL

Slinger seals are available on select series offered by Impro Fluidtek. Slinger seals offer extended shaft/shaft seal protection by prevented a buildup of material around the circumference of the shaft which can lead to premature shaft seal failures. The Impro Fluidtek slinger seals are designed to be larger in diameter than competitive products, providing greater surface speed and 'slinging action'.



Slinger seals are also available on 4-hole flange mounts on select series. Contact a Impro Fluidtek Customer Service Representative for additional information.

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#### **OVERVIEW**

The WH Series motor features a case drain design, making it an ideal choice for medium-duty applications with high duty cycles or frequent direction reversals. This design offers several advantages, such as lowering pressure on the shaft seal and facilitating a cooling loop for the system. Additionally, the case flow helps lubricate essential drive components, enhancing motor longevity. An internal drain option is also available. The motor incorporates a laminated manifold and a three-zone orbiting valve, resulting in improved overall efficiency and greater usable power. Furthermore, a steel-faced seal in the orbiting valve minimizes the risk of seal extrusion or melting, which can occur in competing models.

# **FEATURES / BENEFITS**

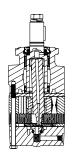
- Three bearing options available, enabling the load-carrying capabilities of the motor to be tailored to specific applications.
- The heavy-duty drive link stands out as the most robust in its category, featuring case flow lubrication that minimizes wear and extends its lifespan.
- Three-zone orbiting valve accurately controls oil flow, delivering outstanding volumetric efficiency.
- The rubber-energized steel face seal is designed to withstand high pressure and temperature without extruding or melting.
- Standard case drain allows reduced pressure on the shaft seal while maintaining driveline lubrication for maximum motor life.

# TYPICAL APPLICATIONS

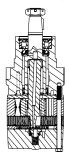
Medium-duty wheel drives, augers, mixers, winch drives, swing drives, grapple heads, feed rollers, broom drives, chippers, mining equipment, forrestry equipment and more

#### **SERIES DESCRIPTIONS**

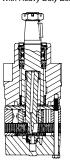
600 - Hydraulic Motor Standard







630 - Hydraulic Motor
With Heavy Duty Bearing



# **SPECIFICATIONS**

CODE	CODE Displacement cm³ [in³/rev]		Speed	Max. Flow lpm [gpm]		Max. Torque Nm [lb-in]		Max. Pressure bar [psi]			
	Citis [iiis/lev]	cont.	inter.	cont.	inter.	cont.	inter.	cont.	inter.	peak	
200	204 [12.4]	465	558	95 [25]	114 [30]	558 [4936]	653 [5778]	207 [3000]	241 [3500]	276 [4000]	
260	261 [15.9]	362	434	95 [25]	114 [30]	746 [6598]	868 [7677]	207 [3000]	241 [3500]	276 [4000]	
300	300 [18.3]	315	378	95 [25]	114 [30]	846 [7485]	978 [8637]	207 [3000]	241 [3500]	276 [4000]	
350	348 [21.2]	272	326	95 [25]	114 [30]	1018 [9010]	1172 [10367]	207 [3000]	241 [3500]	276 [4000]	
375	375 [22.8]	253	303	95 [25]	114 [30]	1088 [9628]	1246 [11029]	207 [3000]	241 [3500]	276 [4000]	
470	465 [28.3]	204	244	95 [25]	114 [30]	1142 [10106]	1362 [12056]	173 [2500]	207 [3000]	241 [3500]	
540	536 [32.7]	176	211	95 [25]	114 [30]	1038 [9188]	1280 [11325]	138 [2000]	173 [2500]	207 [3000]	
750	748 [45.6]	126	151	95 [25]	114 [30]	1040 [9207]	1399 [12382]	103 [1500]	138 [2000]	172 [2500]	

<sup>▶</sup> Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing. Running at intermittent ratings should not exceed 10% of every minute of operation.



22.1 [.872]

mm [in]

143 [1266]

72 [633]

286 [2532] | 429 [3798] | 572 [5064]

Displacement tested at 54°C [129°F] with an oil viscosity of 46cSt [213 SUS]

# **DISPLACEMENT PERFORMANCE**

פוט	PLAC		ENI PER	KFUKIVI	ANCE								
			Pressure - ba	r [psi]	Γ		I	I	Max. Cont.	Max. Inter.	1		
	200		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
	204 cm <sup>3</sup> [12	2.4 in <sup>3</sup> ]	/ rev Torque - Nm [	lb-inl. Speed	rpm				Intermitte	nt Ratings - 1	0% of (	Operation	ı
[md	2 [0.5]		38 [335]	77 [683]								10	균
Flow - Ipm [gpm]	4 [1]		39 [342]	85 [748]	174 [1543]	258 [2284]	329 [2913] <b>5</b>					19	heoretical rpm
ow - I	8 [2]		38 [339]	90 [795]	13 178 [1579]	271 [2396]	361 [3192]	454 [4016]	519 [4594]	562 [4977]		38	al rpn
Ē	15 [4]		35 36 [323]	85 [749]	178 [1576]	28 283 [2506]	378 [3346]	459 [4059]	555 [4909]	636 [5625]		75	
	23 [6]		73	<b>72</b> 78 [690]	<b>69</b> 177 [1562]	273 [2413]	362 [3202]	<b>54</b> 462 [4085]	551 [4880]	35 645 [5711]		112	
	30 [8]			74 [654]	106 172 [1518]	101 268 [2368]	97 357 [3156]	<b>89</b> 469 [4154]	<b>80</b> 558 [4936]	<b>70</b> 653 [5778]		150	
	38 [10]			148	145 168 [1491]	260 [2301]	133 349 [3091]	126 444 [3933]	<b>117</b> 541 [4783]	105 638 [5646]		187	
	45 [12]				184 156 [1381]	178 255 [2256]	174 350 [3096]	<b>167</b> 450 [3985]	<b>156</b> 542 [4793]	144 634 [5607]		224	
	53 [14]				221 150 [1332]	<b>215</b> 251 [2219]	<b>209</b> 330 [2919]	<b>204</b> 435 [3850]	<b>199</b> 526 [4653]	179 638 [5643]		261	
	61 [16]				259 133 [1180]	254 241 [2129]	250 336 [2970]	<b>241</b> 430 [3803]	<b>231</b> 522 [4616]	<b>213</b> 613 [5423]		299	
	68 [18]				<b>297</b> 122 [1082]	<b>293</b> 227 [2012]	286 328 [2899]	<b>278</b> 417 [3692]	<b>276</b> 510 [4510]	<b>256</b> 602 [5329]		336	
	76 [20]				<b>335</b> 112 [993]	<b>332</b> 214 [1897]	325 309 [2732]	<b>319</b> 401 [3547]	<b>310</b> 496 [4391]	<b>298</b> 587 [5198]		373	
	83 [22]				372	<b>371</b> 199 [1757]	<b>365</b> 303 [2680]	356 384 [3401]	348 493 [4358]	<b>337</b> 579 [5121]		410	
	91 [24]					<b>409</b> 184 [1625]	<b>404</b> 285 [2526]	<b>396</b> 380 [3366]	<b>384</b> 474 [4192]	<b>374</b> 562 [4970]		448	
ax. Int.						<b>447</b> 166 [1472]	<b>443</b> 277 [2453]	<b>433</b> 367 [3244]	<b>423</b> 463 [4101]	<b>417</b> 560 [4953]		466	
Max. Max. Inter. Cont.	95 [25] 114 [30]					465	<b>461</b> 219 [1935]	<b>454</b> 332 [2934]	443	432		559	
i ğ	114 [30]		0		4000/ 🖂	40.000/ 5	558	553				559	]
	Rotor Width		Overall Effici Theoretical To		ш	40 - 69%	0 - 39%	· 🔲					
	17.3		56 [494]	112 [987]	223 [1975]	335 [2962]	446 [3949]	558 [4936]	669 [5924]	781 [6911]	1		
	[.682] mm [in]		Displacement								]		
			Pressure - ba				,		Max. Cont.	Max. Inter.			
	260		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
	261 cm <sup>3</sup> [15	5.9 in <sup>3</sup> ]							Intermitte	I nt Ratings - 1	J 0% of (	Operation	1
Έ	0.00.51		Torque - Nm [ 47 [417]	lb-in], <b>Speed</b> 109 [962]	rpm								
Flow - Ipm [gpm]	2 [0.5]		5 51 [454]	4 110 [972]	238 [2104]	355 [3139]	460 [4074]					8	Theoretical
ıdı - w	4 [1]		13 52 [462]	11 113 [1004]	11 242 [2145]	8 367 [3244]	<b>5</b> 485 [4292]	603 [5334]	715 [6323]			15	ical r
Flo	8 [2]		28 49 [430]	<b>27</b> 111 [985]	<b>25</b> 239 [2115]	<b>22</b> 367 [3247]	<b>18</b> 491 [4343]	<b>14</b> 619 [5474]	11 746 [6598]	859 [7600]		30	грm
	15 [4]		<b>57</b> 44 [391]	<b>56</b> 107 [950]	54 234 [2067]	51 364 [3225]	<b>45</b> 487 [4311]	<b>41</b> 617 [5458]	36 738 [6530]	30 854 [7557]		59	
	23 [6]		87	86 100 [884]	83 228 [2016]	<b>78</b> 355 [3146]	72 478 [4230]	<b>67</b> 612 [5418]	60 733 [6487]	<b>54</b> 868 [7677]		88	
	30 [8]			115 90 [797]	113 220 [1947]	107 348 [3080]	103 468 [4143]	95 605 [5351]	89	82 852 [7541]		117	
	38 [10]			145 84 [748]	143 212 [1877]	138 340 [3011]	132 463 [4094]	123 596 [5272]	115 722 [6390]	<b>107</b> 845 [7481]		146	
	45 [12]			<b>174</b> 71 [631]	172 205 [1813]	168 330 [2921]	162 452 [4004]	152 587 [5195]	143 706 [6244]	133 846 [7491]		175	
	53 [14]			203	<b>201</b> 191 [1688]	198 317 [2807]	185 444 [3927]	179 574 [5077]	173 703 [6221]	163 824 [7291]		204	
	61 [16]				231 174 [1540]	228 305 [2698]	223 429 [3798]	214 560 [4952]	203 690 [6111]	196		233	
	68 [18]				261	256	251	246	230	815 [7214] 220		262	
	76 [20]				156 [1383] 290	289 [2558] 289	418 [3700] 282	544 [4817] 268	675 [5977] 262	810 [7166] 247		291	
	83 [22]				143 [1270] 319	275 [2431] 317	405 [3585] 313	533 [4717] 300	659 [5828] 293	787 [6961] <b>277</b>		320	
	91 [24]				131 [1158] 348	255 [2253] 346	387 [3421] 342	515 [4554] 333	613 [5421] 322	769 [6805] <b>311</b>		349	
Max. Max. Inter. Cont.	95 [25]					239 [2115] 362	373 [3301] 357	505 [4471] 348	628 [5559] <b>342</b>	772 [6832] <b>328</b>		364	
Max. Inter.	114 [30]					157 [1388] <b>434</b>	298 [2637] 432	426 [3768] <b>427</b>				436	
	Rotor		Overall Effici	iency - 70 -	100%	40 - 69%	0 - 39%	5				<b>▶</b> F	
	Width		Theoretical To	orque - Nm [lb	-in]		ı	ı	1		1		of p

▶ Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.

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715 [6330] 858 [7596]

1001 [8861]



# **DISPLACEMENT PERFORMANCE**

DIS	PLACI	EMENT PE	RFORM	ANCE							
		Pressure - ba	ır [psi]	I		I		Max. Cont.	Max. Inter.		
	300	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]		
	300 cm <sup>3</sup> [18	-	[lb-in], Speed	rpm				Intermitter	nt Ratings - 1	0% of Operation	1
[md	2 [0.5]	58 [509] <b>5</b>	117 [1039]	253 [2236] 4						7	The
Flow - Ipm [gpm	4 [1]	58 [517] <b>12</b>	122 [1081] 11	266 [2353]	384 [3396] <b>11</b>	509 [4501] <b>9</b>	633 [5599]			13	Theoretical
- wo	8 [2]	58 [516]	128 [1134]		404 3572]	553 [4893]	683 [6045]	813 [7198]		26	al rpm
正	15 [4]	25 56 [491]	132 [1173]		<b>23</b> 417 [3691]	<b>22</b> 553 [4890]	703 [6225]	836 [7397]	<b>20</b> 962 [8513]	51	] =
	23 [6]	50 53 [466]	<b>49</b> 123 [1092]	<b>49</b> 269 [2384]	<b>48</b> 406 [3590]	<b>47</b> 559 [4949]	701 [6207]	<b>43</b> 831 [7356]	<b>42</b> 954 [8445]	76	
	30 [8]	<b>75</b> 44 [386]	<b>75</b> 117 [1036]	<b>74</b> 256 [2263]	<b>73</b> 419 [3710]	<b>71</b> 548 [4847]	707 [6256]	<b>66</b> 846 [7485]	<b>63</b> 974 [8619]	101	
	38 [10]	100	99 107 [947]	<b>97</b> 251 [2222]	<b>96</b> 390 [3448]	<b>95</b> 561 [4961]	<b>93</b> 691 [6119]	88 836 [7396]	<b>85</b> 976 [8637]	127	
	45 [12]		95 [841]	126 238 [2108]	<b>125</b> 400 [3538]	<b>121</b> 529 [4685]	<b>119</b> 696 [6160]	<b>113</b> 833 [7371]	<b>109</b> 969 [8573]	152	
	53 [14]		<b>151</b> 84 [748]	150 232 [2053]	150 366 [3237]	149 530 [4688]	144 676 [5978]	<b>140</b> 825 [7302]	<b>135</b> 964 [8533]	177	
	61 [16]		<b>176</b> 71 [629]	175 217 [1920]	<b>174</b> 370 [3277]	<b>173</b> 508 [4494]	<b>168</b> 654 [5786]	<b>164</b> 803 [7104]	<b>158</b> 952 [8428]	202	
	68 [18]		201	<b>200</b> 202 [1792]	198 339 [2996]	<b>197</b> 503 [4448]	<b>196</b> 645 [5712]	<b>187</b> 781 [6914]	<b>182</b> 933 [8253]	228	
	76 [20]			227 184 [1631]	<b>226</b> 326 [2887]	<b>226</b> 467 [4129]	<b>221</b> 635 [5619]	<b>214</b> 772 [6831]	<b>211</b> 927 [8205]	253	
				<b>252</b> 164 [1449]	<b>251</b> 308 [2726]	<b>249</b> 446 [3943]	<b>244</b> 604 [5346]	<b>236</b> 745 [6592]	<b>230</b> 896 [7926]	278	
	83 [22]			<b>277</b> 147 [1304]	<b>275</b> 286 [2535]	<b>274</b> 437 [3871]	<b>271</b> 580 [5137]	<b>269</b> 723 [6401]	<b>267</b> 861 [7620]	<u> </u>	
× ±	91 [24]			<b>302</b> 116 [1024]	<b>301</b> 291 [2574]	300	<b>296</b> 575 [5085]	<b>293</b> 707 [6255]	<b>285</b> 848 [7500]	303	
x. Max. er. Cont	95 [25]			315	<b>314</b> 204 [1805]	<b>312</b> 347 [3067]	<b>310</b> 499 [4416]	309	302	316	
Max. Inter.	114 [30]				378	376	370			379	
	Rotor Width		iency - 70 - orque - Nm [lb		40 - 69%	0 - 39%					
	25.4	82 [729]	165 [1457]	I .	494 [4371]	659 [5828]	823 [7285]	988 [8742]	1152 [10199]		
	[1.000] mm [in]		t tested at 54°								
		Pressure - ba						Max. Cont.	Max. Inter.		
	350	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]		
	348 cm <sup>3</sup> [21		[lb-in], <b>Speed</b>	rpm				Intermitter	nt Ratings - 1	0% of Operation	1
[mdb	2 [0.5]	69 [606] <b>4</b>	140 [1243] <b>3</b>	262 [2318] <b>2</b>						6	Theo
J wd	4 [1]	75 [660] <b>10</b>	153 [1350] 9	309 [2733] <b>7</b>	454 [4014] 6					11	Theoretical rpm
Flow - lpm [gpm]	8 [2]	75 [667] <b>21</b>	158 [1395] <b>20</b>	325 [2880] <b>17</b>	489 [4326] <b>16</b>	647 [5727] <b>14</b>	784 [6937] <b>13</b>	917 [8119] <b>11</b>		22	ll rpm
	15 [4]	73 [648] <b>43</b>	159 [1405] <b>42</b>	333 [2943] 38	502 [4443] <b>36</b>	677 [5988] <b>33</b>	830 [7342] <b>31</b>		1123 [9935] <b>26</b>	44	
	23 [6]	67 [594] <b>65</b>	152 [1346] <b>63</b>	328 [2901] <b>61</b>	502 [4439] <b>55</b>	670 [5926] <b>51</b>		1010 [8940] <b>49</b>		66	
	30 [8]	56 [494] <b>87</b>			494 [4368] <b>78</b>			1018 [9010] <b>65</b>		88	
	38 [10]						830 [7345] 88			109	
	45 [12]		121 [1068] 130	291 [2578] 128		641 [5672] 115	817 [7231] <b>107</b>		1169 [10342] <b>100</b>	131	
	53 [14]		103 [907] <b>151</b>		452 [4001] <b>145</b>		815 [7212] 130		1162 [10284] <b>115</b>	153	
	61 [16]		85 [755] 174		431 [3818] <b>168</b>		790 [6991] <b>152</b>		1141 [10099] <b>136</b>	175	
	68 [18]		66 [587] <b>196</b>	246 [2174] 193	432 [3823] 190	583 [5161] <b>185</b>	768 [6800] <b>171</b>		1131 [10012] <b>159</b>	197	
	76 [20]				391 [3459] <b>211</b>		750 [6637] <b>196</b>		1101 [9742] <b>176</b>	218	
	83 [22]				372 [3293] <b>236</b>	545 [4825] <b>230</b>	724 [6408] <b>219</b>		1092 [9666] <b>198</b>	240	
	91 [24]			169 [1492] <b>261</b>	349 [3085] 257	537 [4755] <b>253</b>	698 [6179] <b>243</b>	200	100	262	
Aax. Sont.	95 [25]			20.	325 [2874] <b>272</b>	507 [4491] <b>265</b>	687 [6082] <b>254</b>			273	
Max. Max. Inter. Cont	114 [30]				255 [2258] <b>326</b>		605 [5354] <b>315</b>			327	
	Rotor	Overall Effic	iency - 70 -	100%	40 - 69%	0 - 39%					► Performance data is typical. Performance
	Width	Theoretical To	orque - Nm [lb	p-in]		<del>-</del>	_			,	of production units varies slightly from one
	39.4 [1.553]	95 [844]	191 [1688]	381 [3376]	572 [5064]	763 [6752]	954 [8439]	1144 [10127]	1335 [11815]		motor to another. See page 6 for additional information on product testing.
	mm [in]	Displacement	t tested at 54°	C [129°F] wit	n an oil viscos	ity of 46cSt [2	13 SUS]				



39.4 [1.553]

mm [in]

127 [1127] 255 [2253]

509 [4506]

Displacement tested at 54°C [129°F] with an oil viscosity of 46cSt [213 SUS]

# **DISPLACEMENT PERFORMANCE**

DIS	PLACE	MENI PE		ANCE								
		Pressure - b			1			Max. Cont.	Max. Inter.			
	375	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
	375 cm <sup>3</sup> [22.8		[lb-in], Speed	rpm				Intermitte	nt Ratings - 10	1% of	Operation	n
[mdb	2 [0.5]	69 [611] <b>4</b>									6	Theo
Flow - Ipm [gpm]	4 [1]	74 [651] <b>9</b>	161 [1425] 8	330 [2920] <b>8</b>	494 [4369] <b>7</b>	653 [5783] 6	823 [7283] <b>5</b>				11	heoretical
- wol	8 [2]	76 [676] <b>20</b>	173 [1527] <b>19</b>	354 [3133] <b>18</b>	518 [4582] <b>17</b>	685 [6065] <b>15</b>	860 [7611] <b>13</b>	1021 [9038] <b>13</b>			21	T m
ш	15 [4]	73 [649] <b>40</b>	158 [1399] <b>40</b>	350 [3098] 38	535 [4731] <b>37</b>	706 [6250] <b>34</b>		1032 [9130] <b>30</b>	1191 [10541] <b>30</b>		41	1
	23 [6]	66 [588] <b>60</b>	159 [1407] <b>60</b>	346 [3058] <b>59</b>	547 [4841] <b>57</b>	712 [6300] <b>54</b>	899 [7956] <b>49</b>	1080 [9561] <b>47</b>	1231 [10898] <b>45</b>		61	1
	30 [8]	57 [502] <b>81</b>	147 [1301] <b>80</b>	337 [2980] <b>79</b>	537 [4749] 77	700 [6192] <b>74</b>		1088 [9628] <b>65</b>	1236 [10941] <b>62</b>		82	1
	38 [10]	<u> </u>	134 [1190] 101	323 [2856] 100	510 [4512] 99	694 [6139] <b>95</b>	887 [7849] <b>90</b>	1066 [9437] <b>85</b>	1246 [11029] <b>79</b>		102	1
	45 [12]		124 [1097] 121	309 [2730] <b>120</b>	496 [4385] 119	679 [6009] 114		1073 [9493] 104	1244 [11010] <b>99</b>		122	1
	53 [14]		109 [961] 141	290 [2563] 140	477 [4217] 138	680 [6016] <b>136</b>	854 [7556] 130	1041 [9214] 123	1230 [10888] <b>117</b>		142	1
	61 [16]		82 [728] 162	267 [2362] <b>161</b>	453 [4005] <b>159</b>	637 [5641] <b>157</b>		1041 [9209] 144	1209 [10702] <b>136</b>		163	1
	68 [18]		102	248 [2198] 182	434 [3842] 180	619 [5474] <b>175</b>	812 [7190] <b>171</b>	1002 [8864] 165	1148 [10161] <b>162</b>		183	1
	76 [20]			229 [2026] 202	416 [3685] <b>201</b>	600 [5309] 199	790 [6994] <b>192</b>	979 [8664] 183	1145 [10137] <b>180</b>		203	1
	83 [22]			199 [1764] 222	385 [3406] 221	572 [5065] 219	761 [6738]	953 [8435]	1111 [9834]		223	1
	91 [24]			168 [1490]	362 [3204]	566 [5007]	731 [6471]	210	201		244	1
Max. Cont.	95 [25]			243	347 [3073]	554 [4905]	721 [6384]				254	1
Max. N Inter. C	114 [30]				253 261 [2314]	<b>250</b> 440 [3891]	623 [5514]				304	1
≥ <u>-</u>		Overall Effic	ciency - 70 -	- 100%	40 - 69%	301 0 - 39%	300					_
	Rotor Width		Torque - Nm [lb				_					
	31.8 [1.252]	103 [908]	205 [1815]	410 [3631]	615 [5446]	821 [7261]	1026 [9076]	1231 [10892]	1436 [12707]			
	mm [in]	Displacemen	nt tested at 54°	L 'C [129°F] witl	l h an oil viscos	l sity of 46cSt [2	1 213 SUS]					
		Pressure - b	ar [psi]	1	1	1	Max. Cont.	Max. Inter.	1			
	470	17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]				
	465 cm <sup>3</sup> [28.3		[lb-in], Speed	rpm			Intermitte	nt Ratings - 1	0% of Operation	n		
pm]	2 [0.5]	92 [815]	195 [1723]	374 [3306]					5	The		
Flow - Ipm [gpm]	4 [1]	109 [967]	188 [1661]	418 [3701]	615 [5447]				9	heoretical		
ow - I	8 [2]	99 [875]	217 [1924]	440 [3892]	668 [5910]	871 [7709]	1066 [9436]	1227 [10855]	17	al rpm		
Ē	15 [4]	93 [825]	213 [1887]	441 [3906]	688 [6086]		1131 [10008]		33	┦"		
	23 [6]	85 [751]	200 [1771]	434 [3841]	28 686 [6074]		1141 [10098]		49	1		
	30 [8]	72 [635]	186 [1645]	46 422 [3738]	<b>44</b> 659 [5834]			30 1352 [11963]	66	1		
	38 [10]	53 [472]	169 [1493]		61 639 [5657]		1115 [9871]	<b>45</b> 1351 [11958]	82	1		
	45 [12]	81	152 [1348]	<b>79</b> 402 [3561]	<b>77</b> 608 [5377]	<b>74</b> 855 [7563]		<b>59</b> 1340 [11861]		1		
	53 [14]		97 133 [1175]	<b>96</b> 364 [3221]	<b>94</b> 598 [5292]	89 833 [7374]		<b>76</b> 1319 [11673]		$\dashv$		
	61 [16]		114 103 [910]	113 333 [2947]	112 569 [5037]		98 1063 [9410]	<b>90</b> 1294 [11450]		$\dashv$		
	68 [18]		75 [661]	<b>129</b> 305 [2701]	128 555 [4908]	<b>123</b> 764 [6765]	114 1021 [9033]	<b>104</b> 1267 [11214]		$\dashv$		
	76 [20]		146	281 [2489]	<b>143</b> 507 [4490]	745 [6597]	985 [8719]	<b>124</b> 1236 [10940]		$\dashv$		
	83 [22]			<b>163</b> 227 [2011]	<b>162</b> 473 [4189]	<b>156</b> 714 [6322]	948 [8391]	<b>141</b> 1182 [10462]		$\dashv$		
	91 [24]			179 193 [1705]	178 432 [3827]	<b>176</b> 687 [6079]	<b>168</b> 915 [8093]	162	196	$\dashv$		
ax.				194	<b>192</b> 423 [3743]	<b>191</b> 651 [5759]	186 896 [7928]		205	$\dashv$		
Max. Max. Inter. Cont.	95 [25] 114 [30]				<b>204</b> 321 [2840]	<b>201</b> 538 [4761]	<b>191</b> 784 [6938]		205	$\dashv$		
ī, Ā	117 [30]	0		1000/	244	242	238			┙	_	D
	Rotor Width		<b>ciency -</b> 70 - Torque - Nm [lb		40 - 69%	0 - 39%	•				•	Perf of p
	00.4					1	1	1	1			mot

Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.

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764 [6760] | 1018 [9013] | 1273 [11266] | 1528 [13519]

# WH (All Series)

For Medium Duty Applications



# **DISPLACEMENT PERFORMANCE**

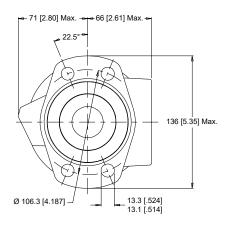
סוט	PLAC	Draggure has [noi]	MANCE		May Cont	May Inter			
	540	Pressure - bar [psi]	69 [1000] 10	04 [4500]	Max. Cont.	Max. Inter.			
	536 cm <sup>3</sup> [3:	17 [250] 35 [500]	09[1000] 10	04 [1500]	138 [2000]	173 [2500]			
	ooo om to	Torque - Nm [lb-in], Spee			Intermitter	nt Ratings - 10	)% of (	Operation	
Flow - Ipm [gpm]	2 [0.5]	108 [953] 215 [1900 3 2						4	Theoretical
<u>md</u> -	4 [1]	107 [946] 225 [1995 6 6	5	0 [6284] <b>5</b>	920 [8138] <b>3</b>			8	etical
Flow	8 [2]	113 [998] 241 [2133 13 12	11	18 [6620] 11	980 [8674] <b>9</b>	1220 [10798] <b>8</b>		15	rpm
	15 [4]	115 [1014] 242 [2137 28 27	26	'9 [6893] <b>25</b>	1038 [9188] <b>24</b>	1266 [11201] <b>20</b>		29	
	23 [6]	102 [902] 234 [2067 42 42	40	38	1019 [9022] <b>36</b>	1274 [11275] <b>32</b>		43	
	30 [8]	89 [792] 222 [1962 56 56	2] 494 [4373] 76 <b>55</b>	64 [6759] <b>52</b>	1020 [9029] <b>48</b>	1280 [11325] <b>43</b>		57	
	38 [10]	71 [630] 201 [1782 70 70	68	66 [6639]	1016 [8994] <b>62</b>	1277 [11299] <b>57</b>		71	
	45 [12]	47 [417] 188 [166 <sup>2</sup> 84 84	455 [4027] 72 <b>84</b>	9 [6455] <b>81</b>	1001 [8858] <b>76</b>	1288 [11394] <b>69</b>		85	
	53 [14]	158 [1397 <b>98</b>	7] 430 [3803] 70 <b>97</b>	96 [6214]	995 [8803] <b>89</b>	1264 [11184] <b>82</b>		99	
	61 [16]	132 [1170 113	0] 403 [3564] 67 112	'0 [5930] <b>110</b>	944 [8353] <b>106</b>	1240 [10970] <b>98</b>		114	
	68 [18]	97 [856] <b>127</b>	366 [3236] 64 <b>127</b>	10 [5664] 126	935 [8276] <b>120</b>	1193 [10557] <b>113</b>		128	
	76 [20]	63 [554] <b>141</b>	335 [2962] 60 140	139 (6345)	878 [7767] <b>135</b>	1156 [10228] <b>129</b>		142	
	83 [22]		303 [2680] 56 <b>155</b>	2 [4972] <b>153</b>	838 [7420] <b>152</b>	1115 [9868] <b>145</b>		156	
	91 [24]			22 [4622] <b>167</b>	813 [7194] <b>164</b>	1075 [9517] <b>161</b>		170	
Max. Cont.	95 [25]			0 [4338] 175	772 [6832] <b>174</b>	1075 [9514] <b>165</b>		177	1
Max. Max. Inter. Cont.	114 [30]			30 [3365] <b>210</b>	659 [5834] <b>209</b>			212	
	Rotor	Overall Efficiency - 7	0 - 100% 40	0 - 69%	0 - 39%				•
	Width	Theoretical Torque - Nm	[lb-in]		_				
	45.5 [1.791]	147 [1302] 294 [2604	588 [5207]   88	33 [7811]	1177 [10414]	1471 [13018]			
	mm [in]	Displacement tested at 5				13 SUS]			
	750	Pressure - bar [psi]		ax. Cont.	Max. Inter.				
	750 748 cm <sup>3</sup> [4:	17 [250] 35 [500]		04 [1500]	138 [2000]				
	THO OIL [H	Torque - Nm [lb-in], Spee	a rpm	ntermitter	nt Ratings - 1	0% of Operation			
Flow - Ipm [gpm]	2 [0.5]	126 [1118] 277 [2450 1 1				3	Theoretical		
<u>- p</u>	4 [1]	156 [1378] 287 [2537 4 3	3	22 [8155] <b>2</b>		6	etical		
Flow	8 [2]	153 [1357] 322 [2853 9 9	8	7	1308 [11579] <b>6</b>	11	md		
	15 [4]	148 [1312] 327 [2898 20 19	18	17	1374 [12161] <b>16</b>	21			
	23 [6]	139 [1230] 323 [2860 30 29	28	27	1393 [12328] <b>25</b>	31			
	30 [8]	123 [1085] 306 [2712 40 40	39	36	1380 [12211] <b>34</b>	41			
	38 [10]	99 [874] 291 [2571 50 49	48	47	45	51			
	45 [12]	75 [664] 274 [2423 60 59	58	57	1392 [12318] <b>55</b>	61			
	53 [14]	46 [408] 239 [2113 <b>70 70</b>	69	68	1372 [12146] <b>64</b>	71			
	61 [16]	190 [1682 <b>81</b>	80	58 [8479] <b>78</b>	1327 [11742] <b>76</b>	82			
	68 [18]	150 [1325 <b>91</b>	5] 535 [4738] 9: 90	21 [8150] <b>88</b>	1299 [11494] <b>86</b>	92			
	76 [20]	107 [949] <b>101</b>	486 [4298] 8° <b>100</b>	78 [7771] <b>100</b>	1253 [11090] <b>97</b>	102			
	83 [22]		111	22 [7273] <b>110</b>	1198 [10598] <b>108</b>	112			
	91 [24]			61 [6736] <b>120</b>	1143 [10117] <b>117</b>	122			
Max. Cont.	95 [25]		369 [3268] 73 126	37 [6523] <b>125</b>	1111 [9830] <b>124</b>	127			
Max. Max. Inter. Cont.	114 [30]			94 [4374] <b>149</b>		152			
		Overall Efficiency - 7		0 - 69%	0 - 39%		_		
	Rotor								
	Rotor Width	Theoretical Torque - Nm	[lb-in]	-					
		Theoretical Torque - Nm 205 [1815] 410 [3631		31 [10892]	1641 [14522]				

<sup>▶</sup> Performance data is typical. Performance of production units varies slightly from one motor to another. See page 6 for additional information on product testing.

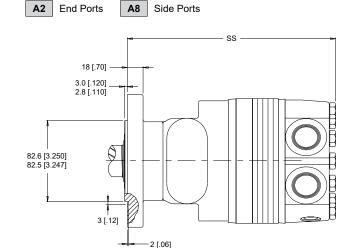


# **HOUSINGS**

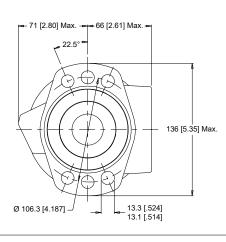
# 4-HOLE, MAGNETO MOUNT



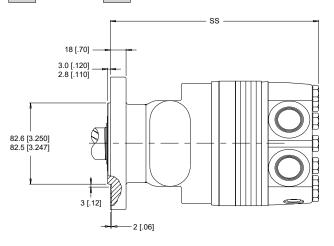
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].



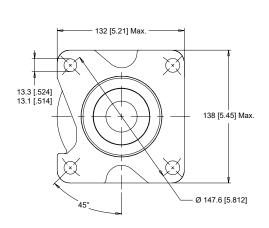
# 6-HOLE, SAE A MOUNT



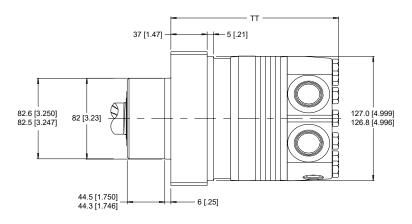




# 4-HOLE, WHEEL MOUNT



# W2 End Ports W8 Side Ports



▶ Dimensions SS & TT are charted on page 22. Porting options listed on pages 23-24.

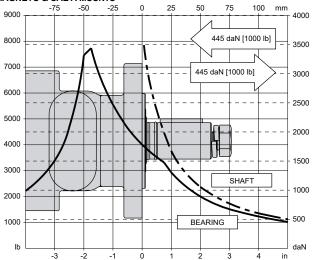


# **TECHNICAL INFORMATION**

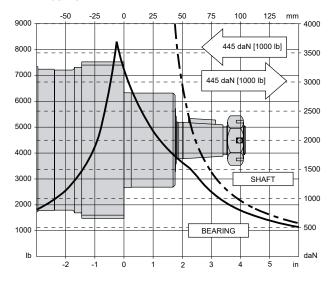
#### ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an  $L_{10}$  life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

#### **MAGNETO & SAE A MOUNTS**



# WHEEL MOUNTS



#### **LENGTH & WEIGHT CHART**

Dimensions SS & TT are the overall motor lengths from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed on page 21.

SS	Endcovers on pg. 21	Endcovers on pg. 22	Weight		
#	mm [in]	mm [in]	kg [lb]		
200	205 [8.08]	208 [8.19]	15.9 [35.0]		
260	210 [8.26]	213 [8.37]	16.3 [36.0]		
300	213 [8.39]	216 [8.50]	16.6 [36.6]		
350	227 [8.95]	230 [9.06]	17.8 [39.2]		
375	219 [8.75]	222 [8.75]	17.1 [37.8]		
470	227 [8.95]	230 [9.06]	17.8 [39.2]		
540	233 [9.18]	236 [9.29]	18.3 [40.3]		
750	251 [9.89]	254 [10.00]	19.7 [43.5]		

TT	on pg. 21	on pg. 22	Weight
#	mm [in]	mm [in]	kg [lb]
200	163 [6.42]	166 [6.53]	13.4 [29.6]
260	168 [6.61]	171 [6.72]	13.9 [30.6]
300	171 [6.74]	174 [6.85]	14.6 [32.2]
350	185 [7.29]	188 [7.40]	15.7 [34.7]
375	177 [6.99]	180 [7.10]	15.2 [33.4]
470	185 [7.29]	188 [7.40]	15.7 [34.7]
540	191 [7.53]	194 [7.64]	16.2 [35.8]
750	209 [8.24]	212 [8.35]	17.7 [39.1]

► All WH series motor weights can vary ± 0.9 kg [2 lb] depending on model configurations such as housing, shaft, endcover, options etc.



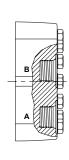
# **PORTING**

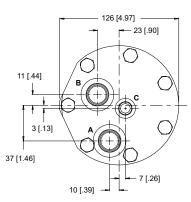
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

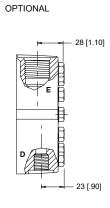
**END PORTED - OFFSET** 

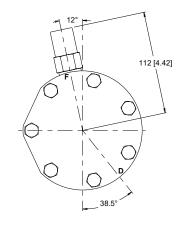
1 Main Ports **A, B**: 7/8-14 UNF Drain Port **C**: 7/16-20 UNF

STANDARD









D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed

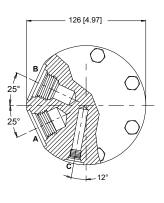
**SIDE PORTED - RADIAL** 

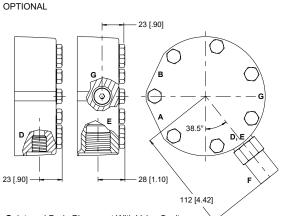
2 Main Ports **A**, **B**: G 3/4
Drain Port **C**: G 1/4

5 Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

STANDARD 36 [1.43]

23 [.90]





D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity

# WH (600 Series)

# Medium Duty Hydraulic Motor



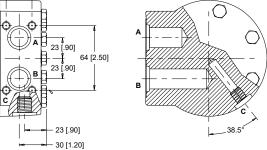
# **PORTING**

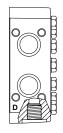
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

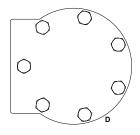
SIDE PORTED - MANIFOLD ALIGNED

Main Ports A, B: 11/16" Drilled
Drain Port C: 7/16-20 UNF

STANDARD OPTIONAL





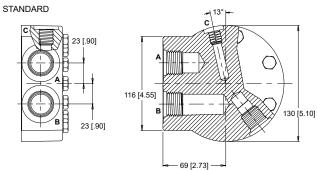


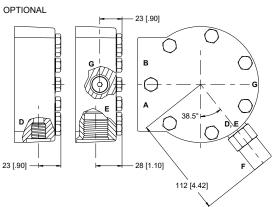
D: Internal Drain

SIDE PORTED - ALIGNED

Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

Drain Port C: G 1/4

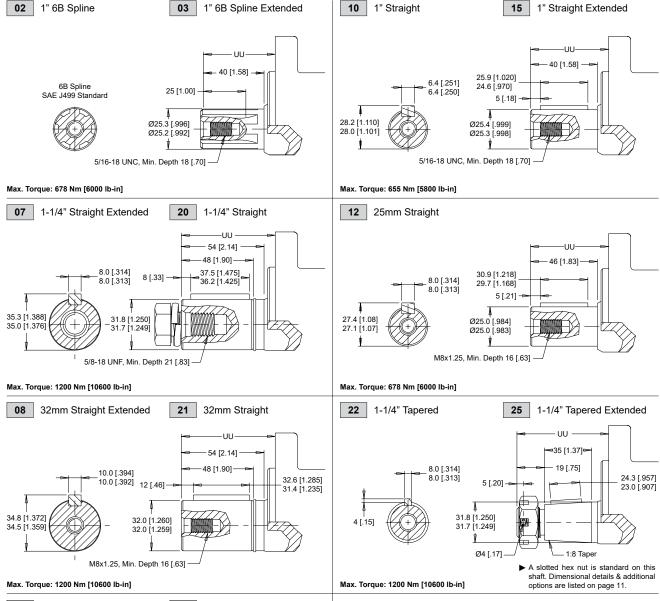


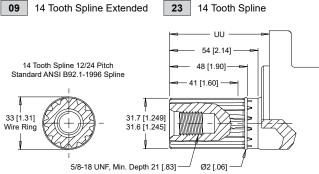


D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity



### **SHAFTS**





Max. Torque: 1200 Nm [10600 lb-in]

# MOUNTING / SHAFT LENGTH CHART

Dimension UU is the overall distance from the motor mounting surface to the end of the shaft and is referenced on detailed shaft drawings above.

٠.		
UU	Magneto & A Mounts	Wheel Mounts
#	mm [in]	mm [in]
02	50 [1.97]	91 [3.60]
03	76 [3.01]	118 [4.64]
07	88 [3.45]	129 [5.09]
08	88 [3.45]	129 [5.09]
09	88 [3.45]	129 [5.09]
10	50 [1.97]	91 [3.60]
12	56 [2.21]	98 [3.84]
15	76 [3.01]	118 [4.64]
20	61 [2.41]	103 [4.05]
21	61 [2.41]	103 [4.05]
22	66 [2.58]	107 [4.22]
23	61 [2.41]	103 [4.05]
25	92 [3.62]	134 [5.26]

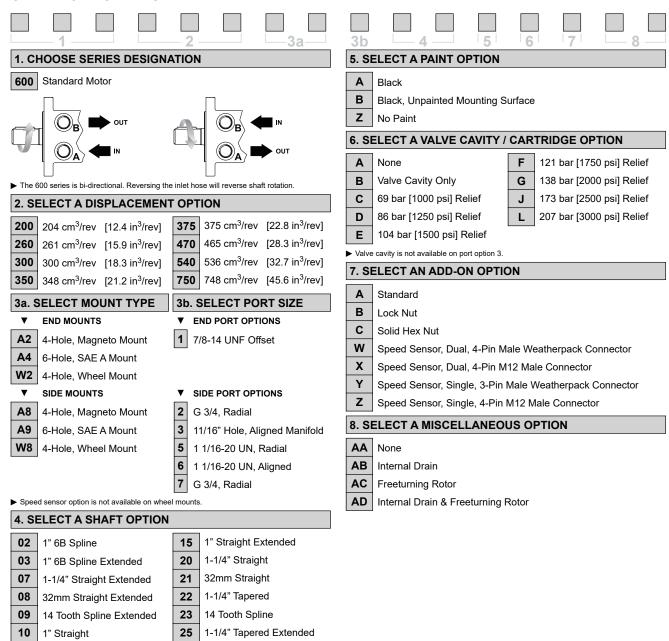
► Shaft lengths vary ± 0.8 mm [.030 in.]

# WH (600 Series)

Medium Duty Hydraulic Motor



#### ORDERING INFORMATION



▶ For options not listed in the table above, please contact us with your requirements

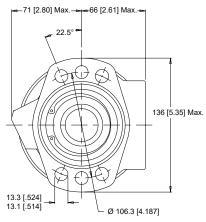
25mm Straight

12



#### **HOUSINGS**

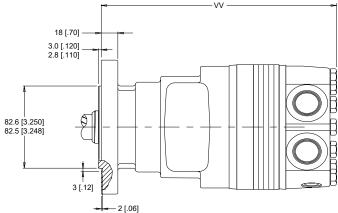
# 6-HOLE, SAE A MOUNT



▶ Porting options listed on pages 28-29.

# ▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].



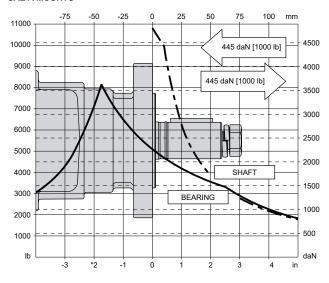


#### **TECHNICAL INFORMATION**

# ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an  $L_{10}$  life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

#### SAE A MOUNTS



#### **LENGTH & WEIGHT CHART**

Dimension VV is the overall motor length from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed above.

► All WH series motor weights can vary ± 0.9 kg [2 lb] depending on model configurations such as housing, shaft, endcover, options etc.

VV	Endcovers on pg. 21	Endcovers on pg. 22	Weight
#	mm [in]	mm [in]	kg [lb]
200	231 [9.08]	234 [9.19]	16.1 [35.4]
260	235 [9.27]	238 [9.38]	16.2 [35.6]
300	239 [9.40]	242 [9.51]	16.9 [37.2]
350	253 [9.95]	256 [10.06]	18.0 [39.6]
375	245 [9.65]	248 [9.76]	17.4 [38.3]
470	253 [9.95]	256 [10.06]	18.0 [39.6]
540	259 [10.19]	262 [10.30]	18.5 [40.7]
750	277 [10.90]	280 [11.01]	20.0 [44.0]

# WH (620 Series)

# Medium Duty Hydraulic Motor



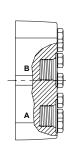
# **PORTING**

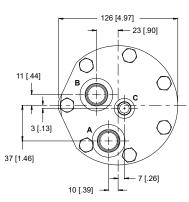
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

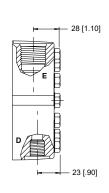
**END PORTED - OFFSET** 

1 Main Ports A, B: 7/8-14 UNF
Drain Port C: 7/16-20 UNF

STANDARD

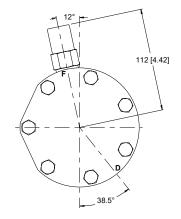






OPTIONAL

OPTIONAL



D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed

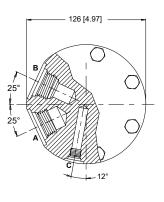
**SIDE PORTED - RADIAL** 

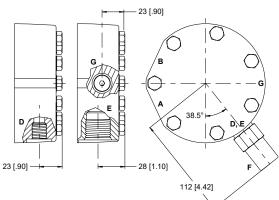
2 Main Ports A, B: G 3/4
Drain Port C: G 1/4

5 Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

STANDARD 36 [1.43]

23 [.90]





D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity



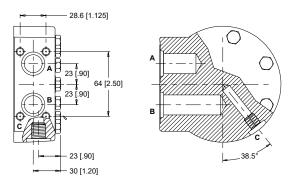
# **PORTING**

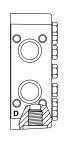
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

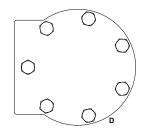
SIDE PORTED - MANIFOLD ALIGNED

Main Ports A, B: 11/16" Drilled
Drain Port C: 7/16-20 UNF

STANDARD OPTIONAL







D: Internal Drain

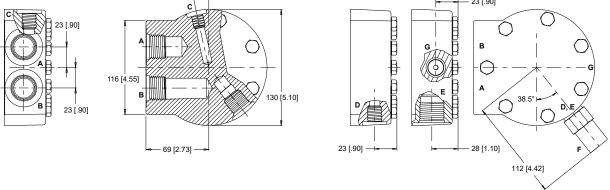
SIDE PORTED - ALIGNED

6 Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

Drain Port C: 7/16-20 UNF

OPTIONAL

23 [.90]



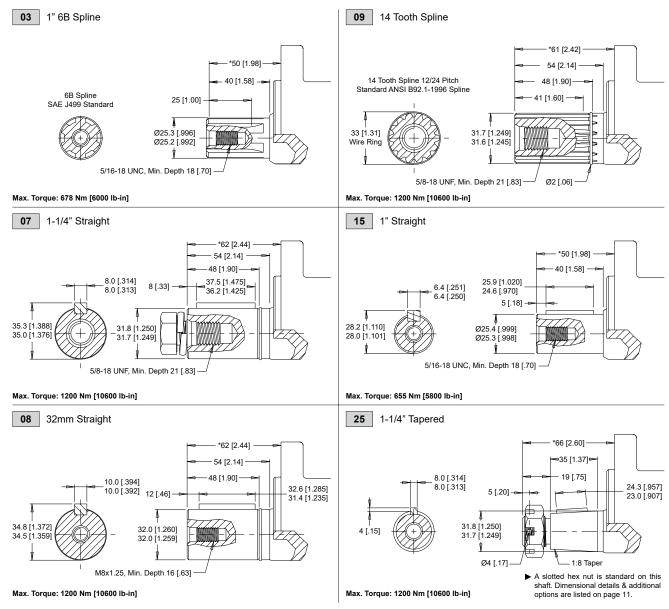
D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity

# WH (620 Series)

# Medium Duty Hydraulic Motor



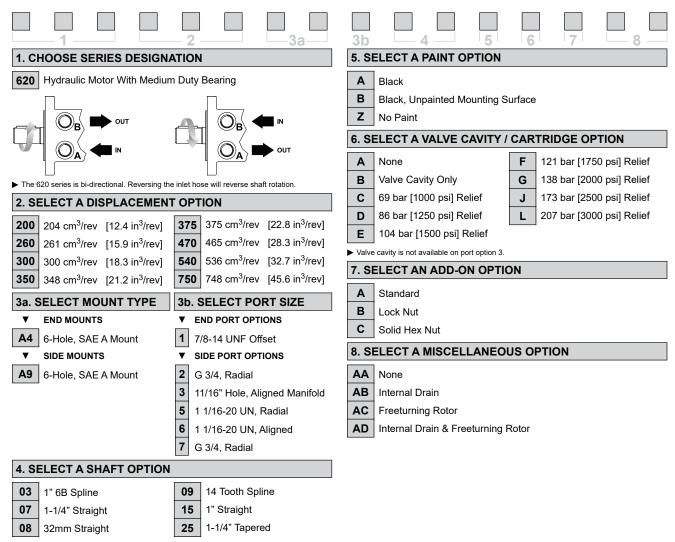
#### **SHAFTS**



► Shaft lengths vary ± 0.8 mm [.030 in.]



# **ORDERING INFORMATION**

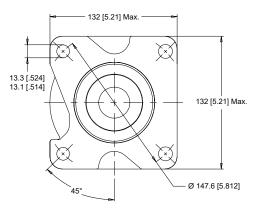


▶ For options not listed in the table above, please contact us with your requirements

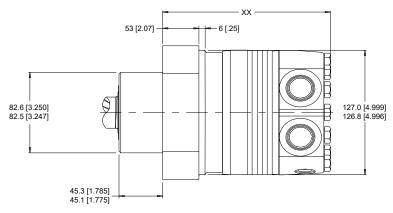


# **HOUSINGS**

#### 4-HOLE, WHEEL MOUNT



W2 End Ports W8 Side Ports



▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

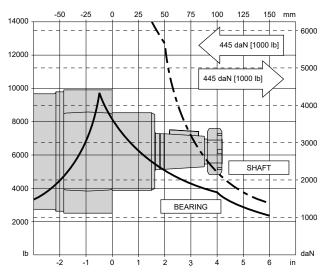
▶ Porting options listed on pages 33-34.

#### **TECHNICAL INFORMATION**

#### ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an  $L_{10}$  life of 2,000 hours at 100 RPM. Radial loads for speeds other than 100 RPM may be calculated using the multiplication factor table on page 7.

# WHEEL MOUNTS



#### **LENGTH & WEIGHT CHART**

Dimension XX is the overall motor length from the rear of the motor to the mounting flange surface and are referenced on detailed housing drawings listed above.

► All WH series motor weights can vary ± 0.9
kg [2 lb] depending on model configurations
euch as housing shaft andcover ontions atc

XX	Endcovers on pg. 21	Endcovers on pg. 22 Weight	
#	mm [in]	mm [in]	kg [lb]
200	199 [7.75]	202 [7.86]	17.5 [38.5]
260	204 [8.04]	207 [8.15]	17.9 [39.5]
300	207 [8.17]	210 [8.28]	18.2 [40.1]
350	221 [8.72]	224 [8.83]	19.3 [42.6]
375	214 [8.42]	217 [8.53]	18.7 [41.2]
470	221 [8.72]	224 [8.83]	19.3 [42.6]
540	227 [8.96]	230 [9.07]	19.8 [43.7]
750	245 [9 67]	248 [9 78]	21 3 [47 0]



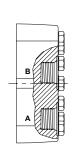
# **PORTING**

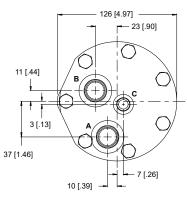
▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

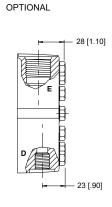
**END PORTED - OFFSET** 

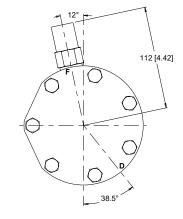
1 Main Ports A, B: 7/8-14 UNF
Drain Port C: 7/16-20 UNF

STANDARD









D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed

**SIDE PORTED - RADIAL** 

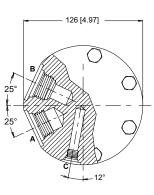
2 Main Ports **A, B**: G 3/4
Drain Port **C**: G 1/4

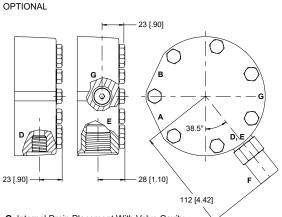
Main Ports A, B: 1 1/16-20 UNDrain Port C: 7/16-20 UNF

STANDARD

36 [1.43]

23 [.90]





D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity

# WH (630 Series)

# Medium Duty Hydraulic Motor



# **PORTING**

▶ Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

SIDE PORTED - MANIFOLD ALIGNED

23 [.90]

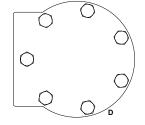
- 23 [.90] - 30 [1.20]

64 [2.50]

Main Ports A, B: 11/16" Drilled
Drain Port C: 7/16-20 UNF

STANDARD OPTIONAL

28.6 [1.125]



D: Internal Drain

SIDE PORTED - ALIGNED

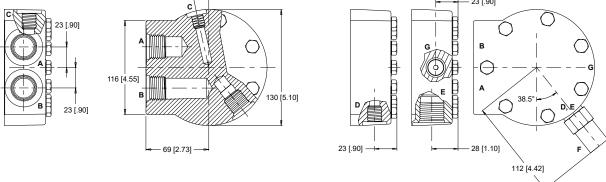
6 Main Ports A, B: 1 1/16-20 UN
Drain Port C: 7/16-20 UNF

7 Main Ports A, B: G 3/4
Drain Port C: 7/16-20 UNF

OPTIONAL

23 [.90]

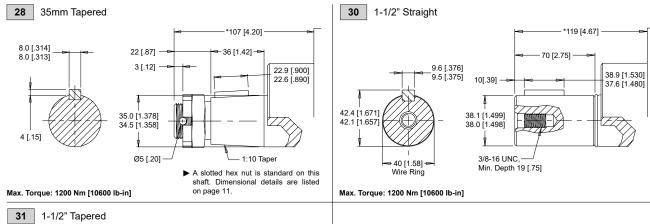
23 [.90]

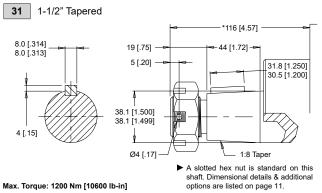


D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF F: Valve Cartridge Installed G: Internal Drain Placement With Valve Cavity



# **SHAFTS**





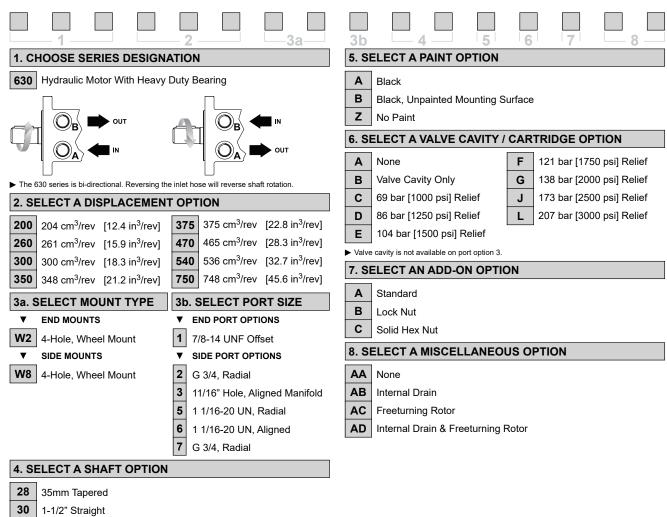
► Shaft lengths vary ± 0.8 mm [.030 in.]

# WH (630 Series)

Medium Duty Hydraulic Motor



# **ORDERING INFORMATION**



▶ For options not listed in the table above, please contact us with your requirements

31

1-1/2" Tapered



# USA

400 E. Diehl Road, Suite 500 Naperville, IL 60563 USA

Email:sales.americas@improfluidtek.com

# Luxembourg

10 Boulevard Royal, 2449 Luxembourg

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No.18, Furong Road 5 Xishan Economy Development Zone Wuxi, Jiangsu China Email:sales.apac@improfluidtek.com